

CompTest 2023

Investigation of transverse matrix cracking in fatigue for laminated composites

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Aloha Airline Flight 243, 1988

❖ Advantages of predictive models

- Cut experimental costs,
- Reduce design delays,
- Sustainability: enhanced structure fatigue life

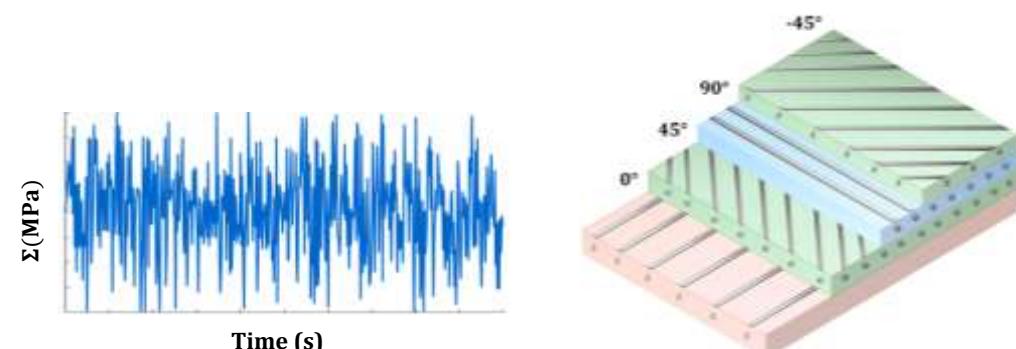
❖ Developing predictive models

- For complex, realistic loadings,
- Prediction for multiaxial laminates

[Kaminski 2015]

- ❖ **A main industrial challenge**
- Efficiently designing lighter structures,
 - Being competitive,
 - Ensuring optimum performances and safety

Necessity of sizing composites in fatigue
and developing predictive models





AMADE headquarters, Girona

❖ **Objectives:**

- Better understanding of laminates fatigue behavior,
- Conduct a complete experimental campaign on a currently in-use material (IMA/M21ev),
- Develop a simple damage model for static and fatigue damage prediction

❖ EXPERIMENTAL CAMPAIGN



Tensile test experimental set up on the IMA/M21ev

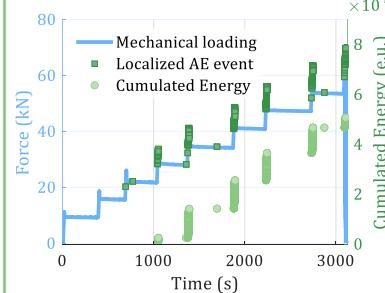
❖ Material

- IMA/M21ev : thermoset, epoxy and continuous carbon fibers, reinforced at the interface

❖ Campaign elaboration

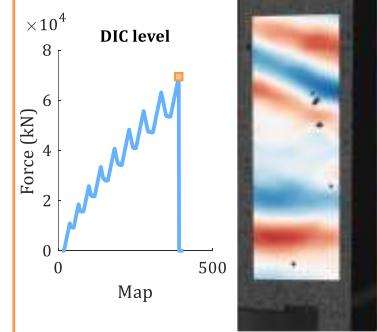
- Definition of stacking sequences: academic and industrial (15 layups),
- Definition of tests to build and validate the model (60 tests),
- Highly instrumented

❖ Acoustic Emission



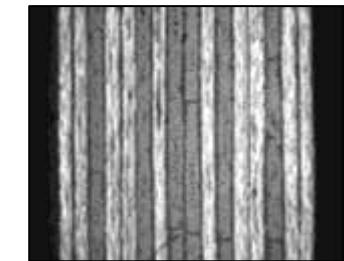
✉ [Hurmane 2015]

❖ Digital Images Correlation



✉ [Hild and Roux 2012]

❖ Optic microscopy



✉ [Huchette 2005], [Nicol 2023]

❖ AUTOMATED CRACK DETECTION TOOL

➤ Deepflow computer vision algorithm

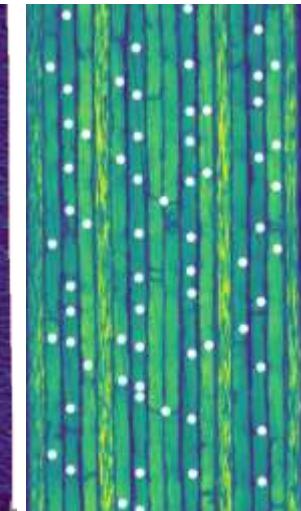
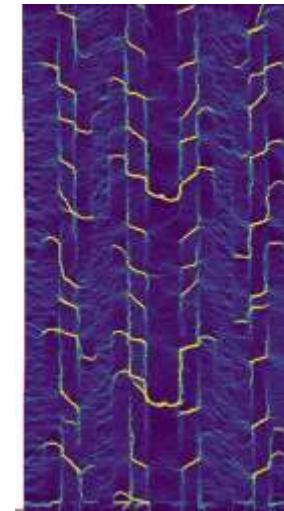
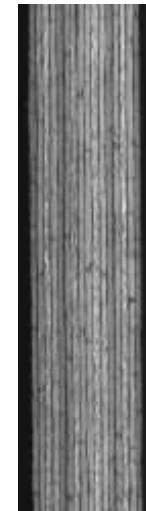
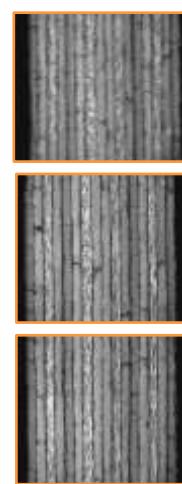
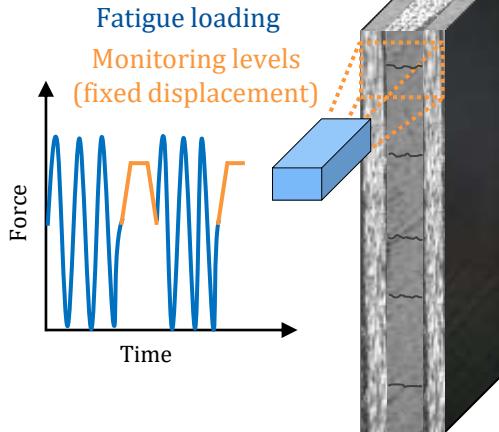
[Nicol et al. 2023]

Microscopic takes under loading

Reconstitution

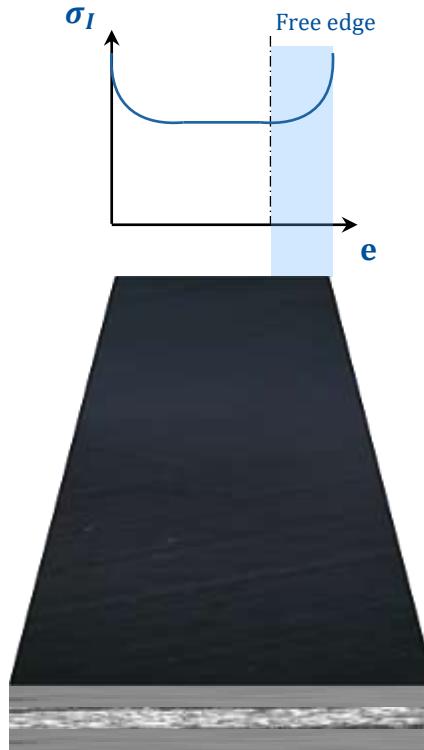
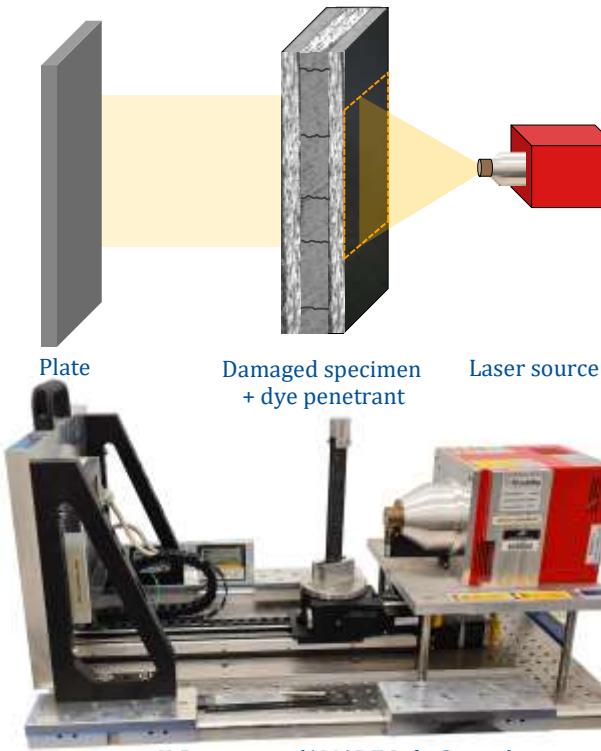
Displacement gradients

Crack detection



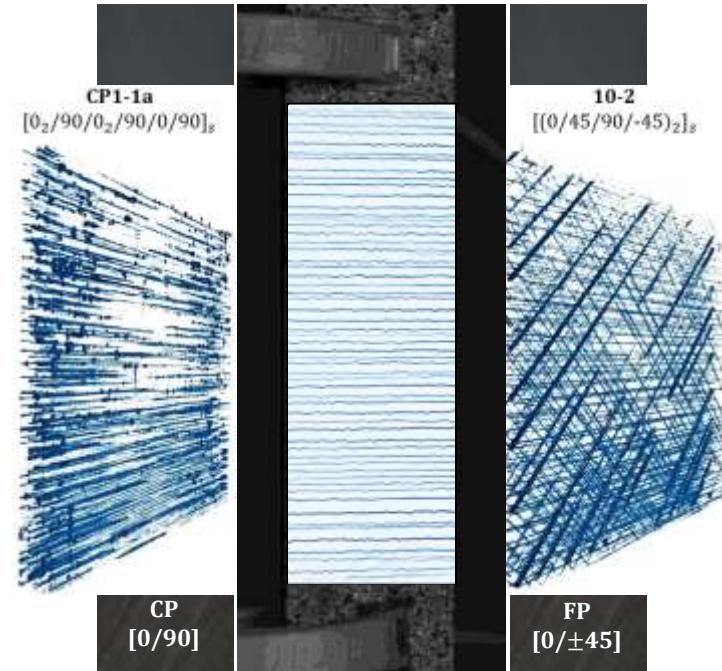
❖ Normalized crack density: $\bar{\rho} = \frac{N_{cracks}}{L_{obs}} e$

❖ FREE EDGE EFFECT



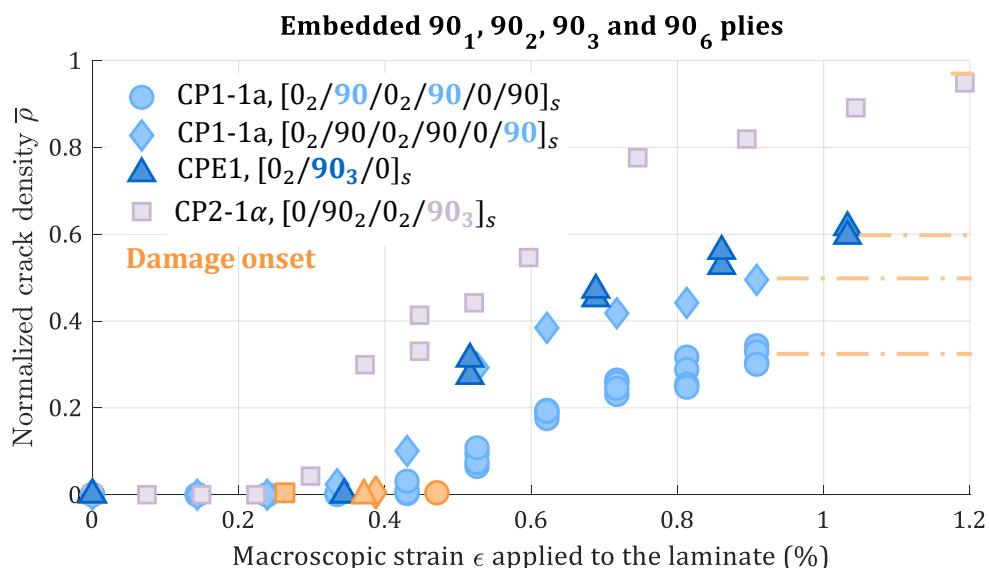
- Overall validity of edge observations for this material

Deepflow



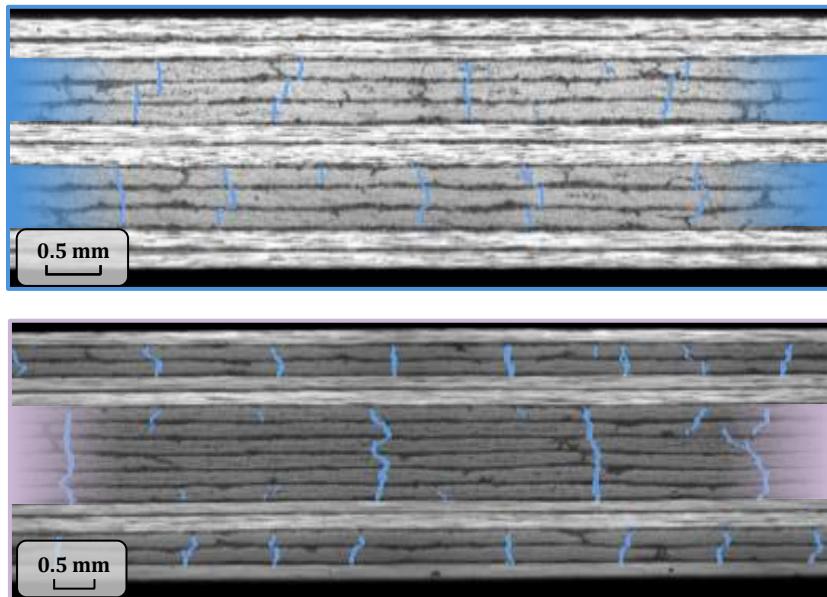
❖ STATIC RESULTS

➤ Ply thickness effect



- Different damage onsets, [Parvizi 1978], [Camanho 2006]
- Different damage evolutions and apparent saturation

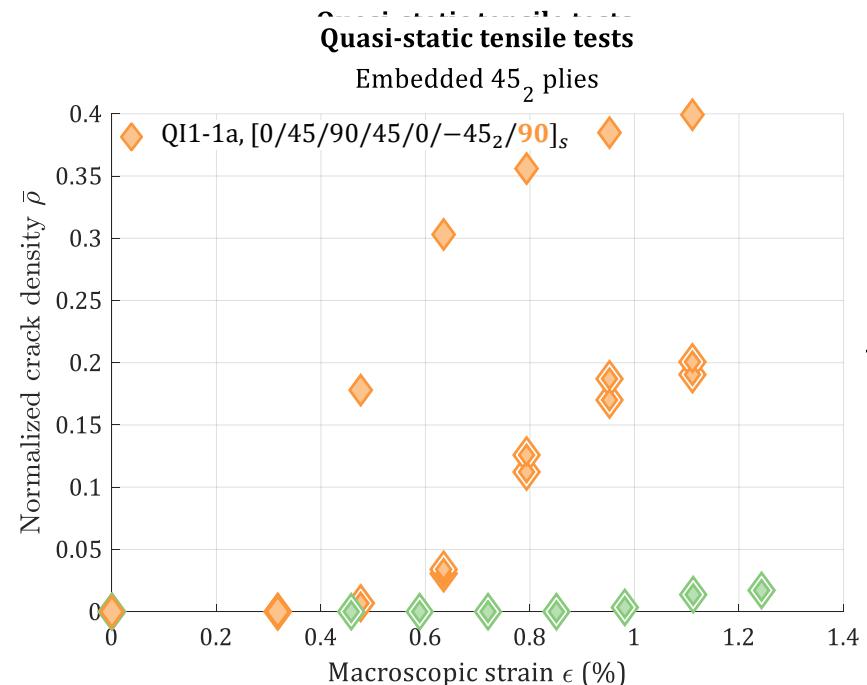
➤ Ply thickness effect



Partial cracks were detected but not counted

❖ STATIC RESULTS

➤ Stacking sequence effect



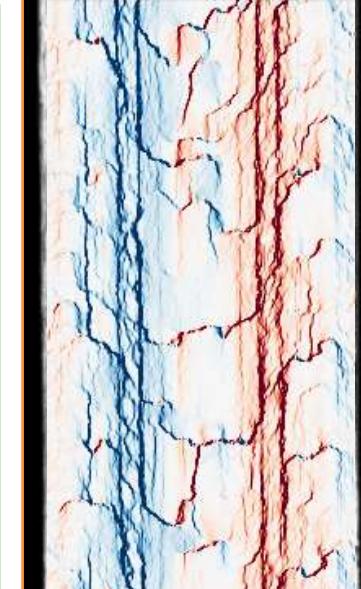
FP1-1a
45
45
0
-45
0
45
0
-45
-45
0
45
0
-45
0
45
45

- Different damage onsets,
- Shear strains inducing microdelaminations $\bar{\mu}$
- Influence of neighboring plies

Shear gradient yx



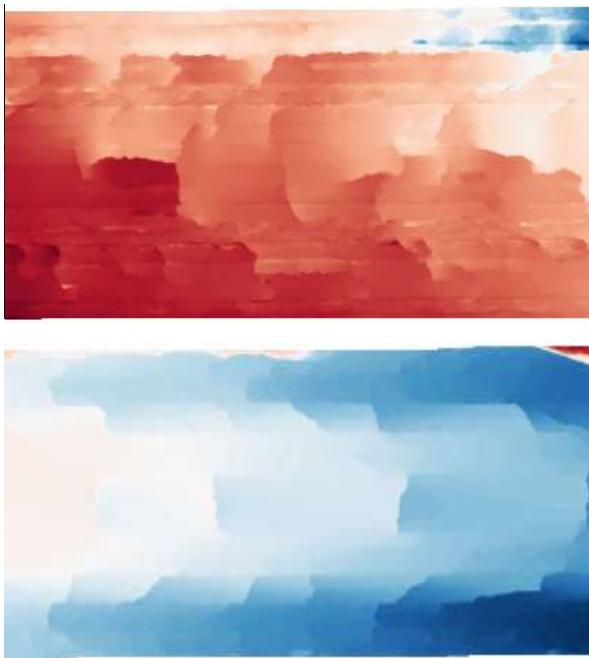
Shear gradient yx



QI1-1a
0
45
90
45
0
-45
-45
90
90
-45
-45
0
45
90
45
0

❖ STATIC RESULTS

➤ Stacking sequence effect



1	2	3	4
14-1	10-1	QI1-1a	OR1-1a
90	0	0	0
-45	45	45	90
0	90	90	45
45	-45	45	45
90	0	-45	90
-45	45	-45	90
0	90	90	-45
45	-45	-45	0
45	-45	90	-45
0	90	90	90
-45	-45	-45	90
90	90	90	90
45	45	45	-45
45	0	0	0
90	0	0	-45
-45	45	45	90
90	90	90	90
45	45	45	45
90	0	0	90

❖ Influence of neighboring plies

Promoted by:

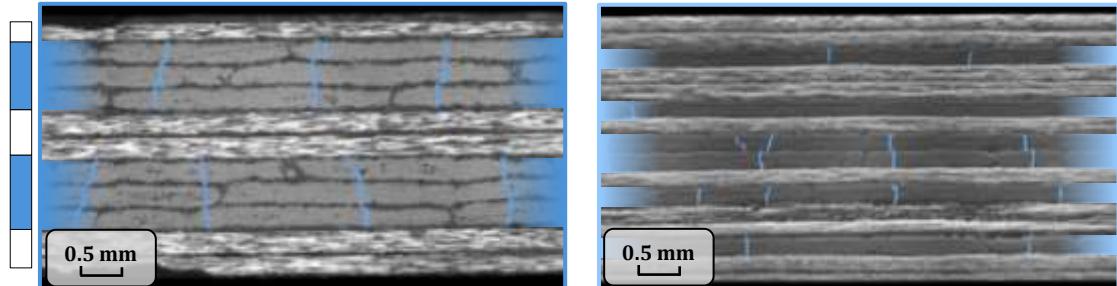
- Thick 90° neighboring plies with an earlier damage onset,
- Propagation of cracks between plies

➤ Necessity of integrating the stacking sequence effect into design rules

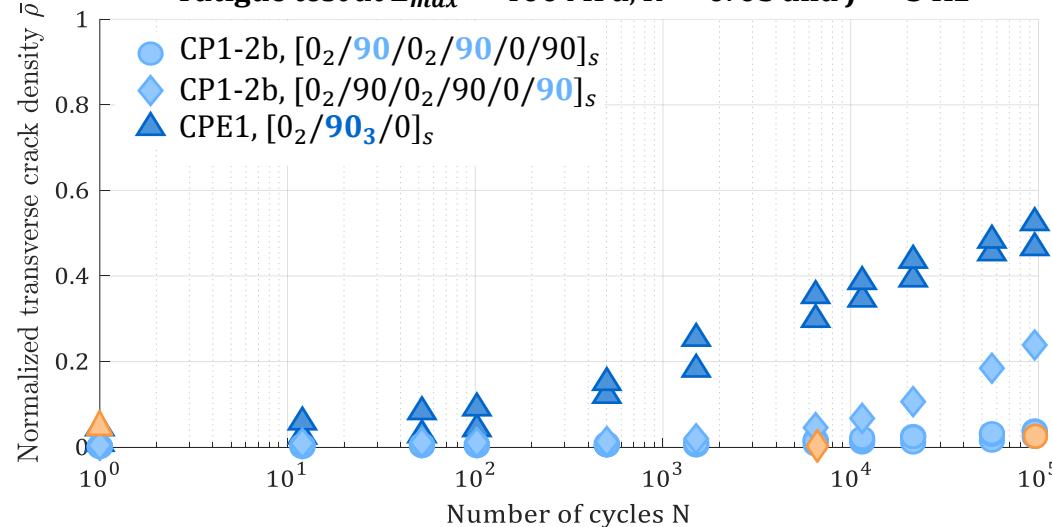
FATIGUE RESULTS

➤ Ply thickness effect

➤ Ply thickness effect on thresholds in fatigue

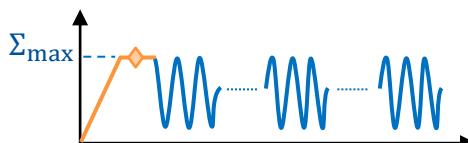


Fatigue test at $\Sigma_{max} = 400$ MPa, $R = 0.05$ and $f = 5$ Hz

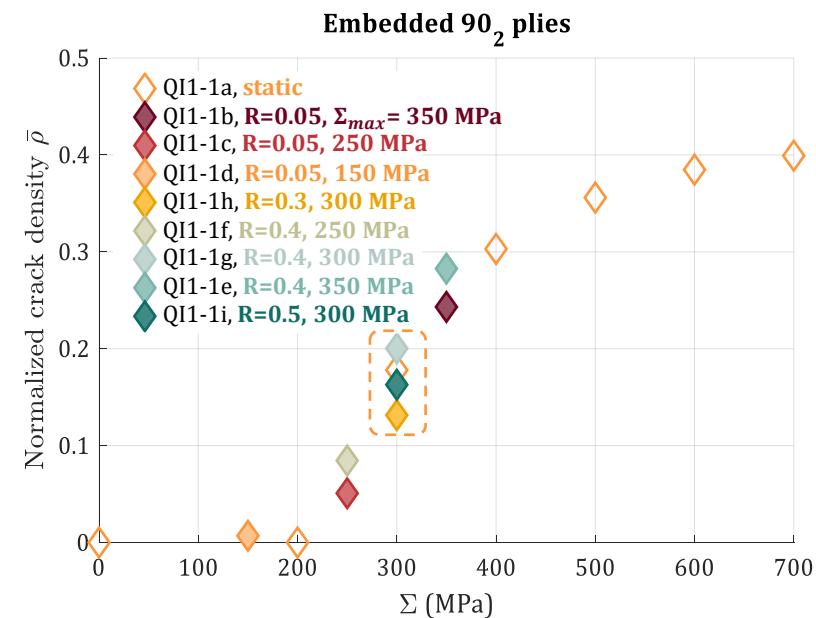


FATIGUE RESULTS

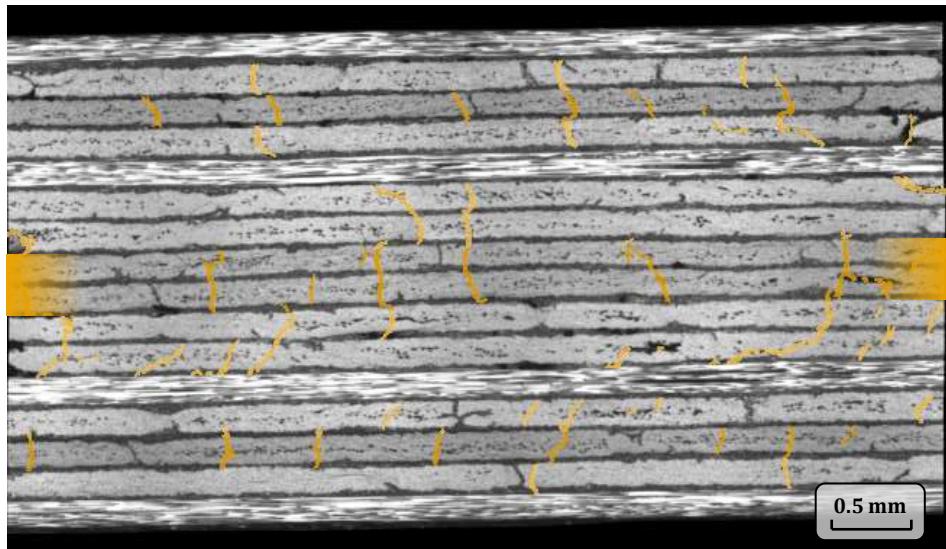
➤ Static and fatigue consistance



➤ Low fatigue dispersion after first static loading



QI1-1h
0
45
90
45
0
-45
-45
90
90
-45
-45
0
45
90
45
0

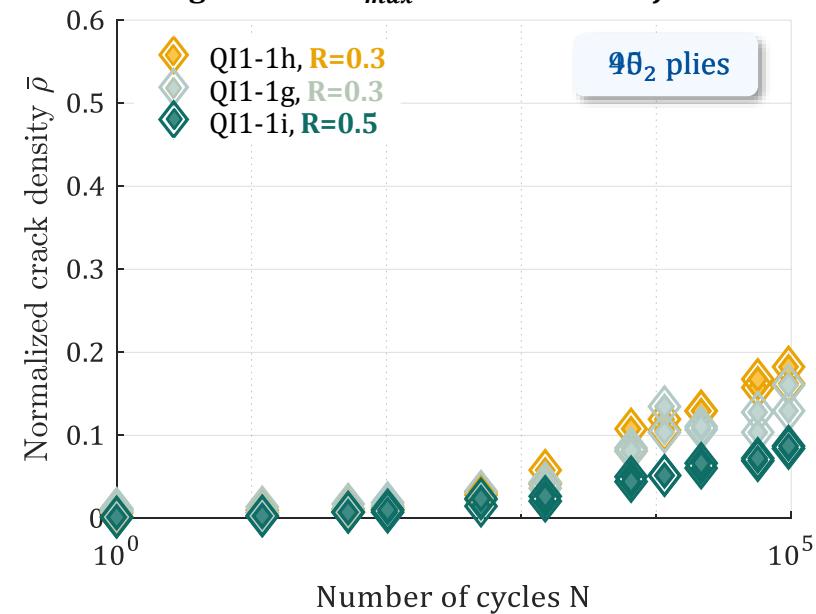


❖ FATIGUE RESULTS

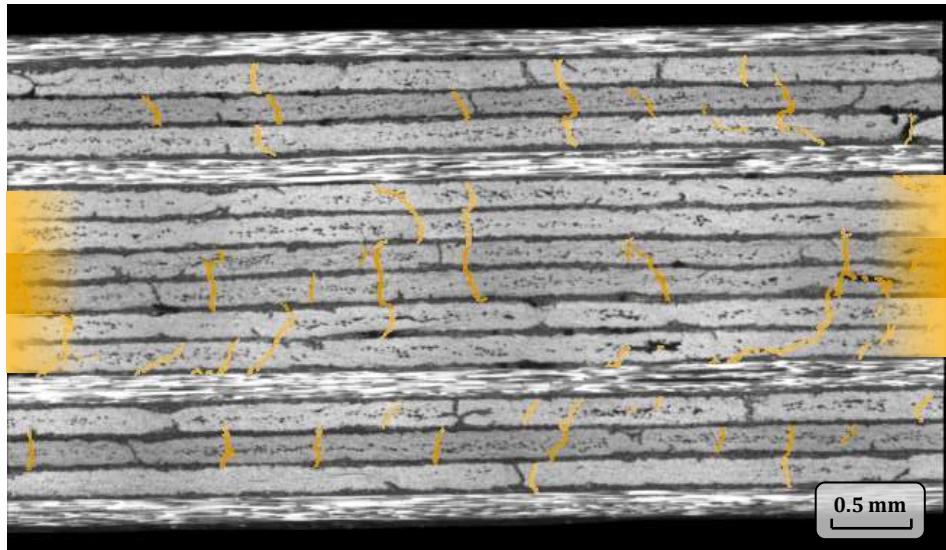
➤ Stress ratio effect

- Low stress ratio effect
- CT-scans planned

Fatigue test at $\Sigma_{max} = 300$ MPa and $f = 5$ Hz



QI1-1h
0
45
90
45
0
-45
-45
90
90
-45
-45
0
45
90
45
0



PERSPECTIVES

Conclusions

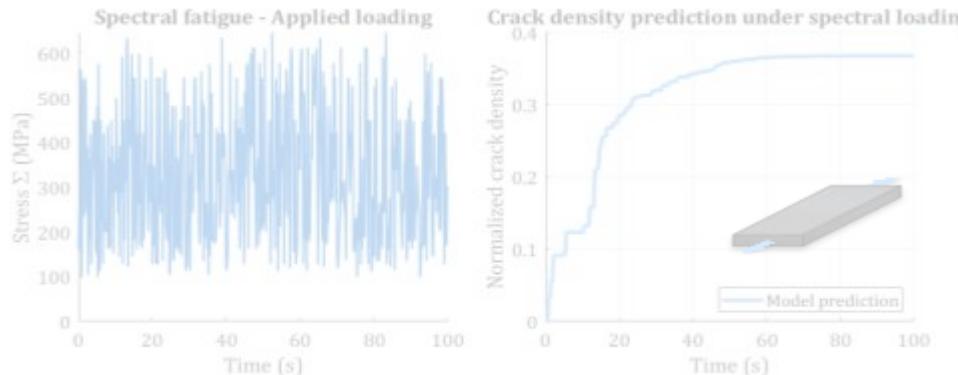
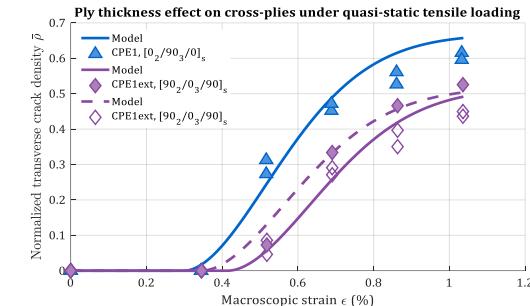
Static and fatigue tests conducted on academic and complex layups,

- Damage onset: ply thickness and neighboring plies,
- Damage evolution: Fatigue tests at different Σ_{max} and stress ratios,
- Quantitative data generated (>70 000 cracks counted)

Development of an incremental damage model based on $\bar{\rho}$ for static and fatigue

Perspectives

- In implementation: cumulative damage effect,
- Spectral fatigue tests planned for validation



THANK YOU FOR YOUR ATTENTION

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Plates	Stacking sequences	Plates	Stacking sequences
Cross-ply laminates (CP1, CP2, CP3)	[0 ₂ /90/0 ₂ /90/0/90] _s [90 ₂ /0/90 ₂ /0/90/0] _s	[0/ \pm 45] laminates (FP1, FP2, FP3)	[45 ₂ /0/-45/0/45/0/-45] _s [45/0/-45/0/45/0/-45] _s
	[90/0 ₂ /90 ₂ /0 ₃] _s [0/90 ₂ /0 ₂ /90 ₃] _s		[0/-45 ₂ /45/0/45/0/45] _s
	[0/90 ₃ /0]		[0/45 ₃ /0/-45 ₃] _s
QI laminates (QI1)	[0/45/90/45/0/-45 ₂ /90] _s	Double-double (DD1)	[60/20/-20/-60 ₂ /20/20/60] _s [-60/60/20/-20/-60/60/20/-20] _s
Oriented laminates (O1)	[0/90/45 ₂ /90 ₂ /-45/0/-45/90 ₂] _s		[30/70/-70/-30 ₂ /70/30] _s [-30/30/70/-70/-30/30/70/-70] _s

❖ MODELING APPROACH

Model at ply scale:
predictive for different
stacking sequences



📖 [Angrand 2016], [Sally 2020], [Germain 2020]

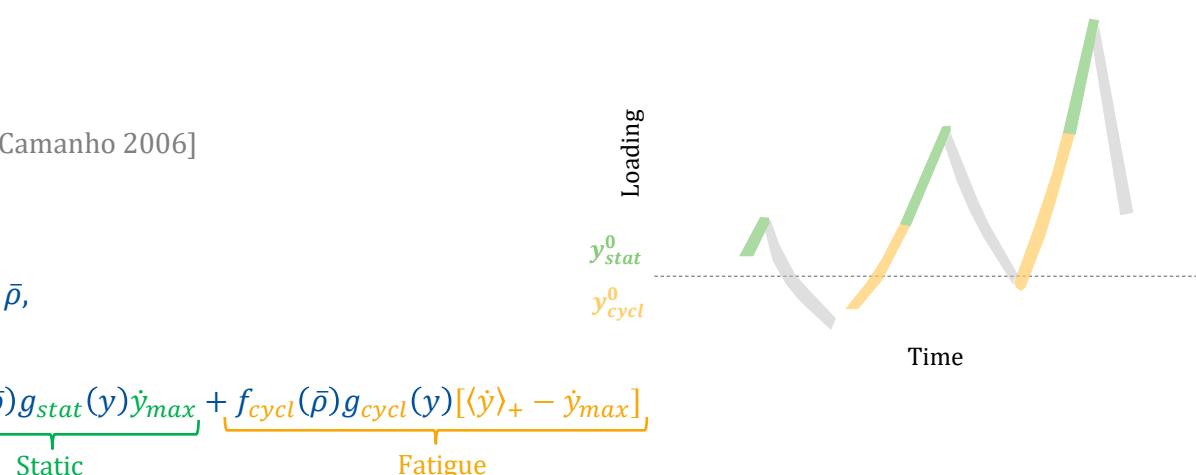
❖ Damage initiation

- Residual thermal stresses,
- Ply thickness effect 📖 [Dvorak 1987], [Camanho 2006]

❖ Damage evolution

- Damage driving force y and crack density $\bar{\rho}$,
- Effect of damage \tilde{S} ,
- Generalized cracking kinetics: $\dot{\bar{\rho}} = \underbrace{f_{stat}(\bar{\rho})g_{stat}(y)\dot{y}_{max}}_{\text{Static}} + \underbrace{f_{cycl}(\bar{\rho})g_{cycl}(y)[\langle \dot{y} \rangle_+ - \dot{y}_{max}]}_{\text{Fatigue}}$

❖ Identification

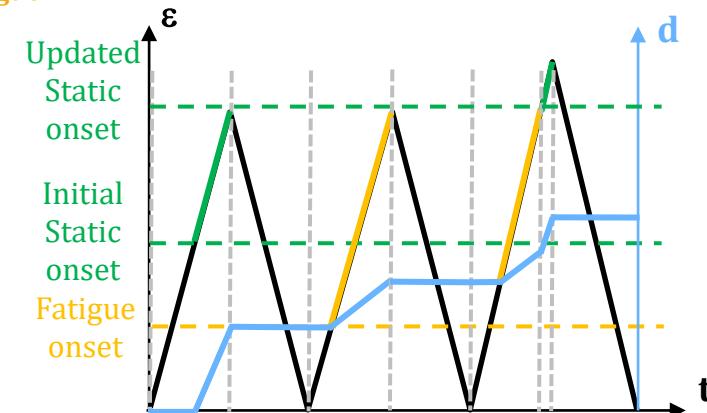


DAMAGE EVOLUTION

❖ Generalized cracking kinetics: $\dot{\rho} = \underbrace{f_{stat}(\bar{\rho})g_{stat}(y)\dot{y}_{max}}_{\text{Static}} + \underbrace{f_{cycl}(\bar{\rho})g_{cycl}(y)[\langle\dot{y}\rangle_+ - \dot{y}_{max}]}_{\text{Fatigue}}$

Presentation of the material approach

- One unique damage variable for each damage mechanism
[Lemaitre 92], [Cantournet 02], [Angrand 16], [Sally 20]
- Continuous damage evolution for static and fatigue loadings
- Fatigue formulation depends on maximal equivalent strain



Unloading:

$$\begin{cases} \dot{y}_{max} = 0 \\ \langle\dot{y}\rangle_+ - \dot{y}_{max} = 0 \end{cases}$$