

MICROCRACKING OF CFRP COMPOSITES DURING CRYOGENIC THERMAL CYCLING



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Hydrogen as an Alternative Fuel

Relative Mass And Size of Different Fuels		
	Gravimetric energy density	Volumetric energy density
Jet fuel	1 (1)	1
Lithium-ion battery	60	18
700 Bar Hydrogen	0.35 (7)	8
Liquid Hydrogen	0.35 (0.5)	4

Values in brackets account for tank weight assuming composite hydrogen tanks.

Why Liquid Hydrogen? Minimised mass and size compared to other alternatives



LH2 Tank Schematic

Why Composites? Literature and modelling predict around 50% weight saving for composite inner skin over a Type I Al-Li baseline. (Vickers, 2013)

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Stresses in Cryogenic Composite Tanks

Thermal Stress

Coefficient of Thermal Expansion (CTE) is a challenge in composite materials as the constituents can have opposing CTE.

- **Carbon Fibres** Negative CTE axially Elongate on cooling.
- **Polymer Matrices** Positive CTE Contract on cooling.
- **Ply Level** interaction between fibres and matrix.
- Laminate level interaction between plys at different angles.

Mechanical

- Internal Pressure in the region of 2-10 bar
- Fluid sloshing during 9g crash case

Role of constituents in composite LH2 tank

Fibres experience the majority of the mechanical stress from the pressure loading.

Matrix experience transverse thermally induced stress from the fibres expanding.

Adding more fibres does not improve performance, it increases the transverse matrix stresses!



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Micro-Cracking

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- Constituents expand and contract relative to each other leading to Internal stresses.
- Polymers become brittle at cryogenic temperatures.
- Material damage occurs through matrix microcracking.

The Microcracking Problem

A fully linked network of microcracks in a tank will enable permeation of hydrogen

Any surface microcracks may cause catastrophic failure if hydrogen becomes trapped during warming









Cryogenic Composite Screening Methods

- **Resistance to cryogenic microcracking** The primary factor for assessing the suitability of composite materials for use in cryogenic tanks.
- Thermal cycling followed by microcrack inspection The most common screening method In literature.
- Thermal Cycling Methods Vary in literature.

Cooling fluid

- LN₂
- LHe

Cooling Method

- Immersion
- Vapour cooling

Heating method

- Elevated
- Ambient

Cycle time

- Cooling rate
- Heating rate

Areas Investigated

Cycle temperature

- Lower temperature
- Upper temperature

Coupon geometry

- Shape
- <mark>Size</mark>





Cooling Methods

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Immersion No cooling rate control – thermal shock Lower temperature fixed to that of the cryogenic fluid

Vapour Dipping Control of cooling rate and lower temperature



LHe Vapour Dipping







Film Boiling in immersion





Video of film boiling on coupon

Film Boiling

Cooling rate influence by film boiling, reduces heat transfer between fluid and object



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Double Walled Glass Beaker

LN2 has faster cooling rate then LHe

Immersion



Cooling Methods



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Specimens

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- Plate specimens with two polished edges to inspect for microcracks with optical microscopy
- Layup
 - 16 Ply QI Blocked
 - [0₂/45₂/-45₂/90₂]_s
- Sizes
 - 25 mm x 25 mm
 - 75 mm x 75 mm
 - 150 mm x 150 mm
- Materials
 - Multiple thermoset and thermoplastic materials tested







Two Materials Presented

Initial

Low Quality





Low Quality material has more porosity / Voids High Quality material has increased toughening







Effects of LN2 Immersion – Low Quality Material 25mm



microcracking

For testing purposes, a low quality material was made with stress raisers and defects to generate microcracking.

Significant microcracking occurred when cooled rapidly at 15 K/s to 77K.







Effects of LHe Cycling – Low Quality Material 25mm



In comparison when cooled slowly at 0.5 K/s to 20K reduced microcracking was visible, in some coupons there were no microcracks.







Effects of LN2 Immersion – High Quality Material 25mm



No Cracking in high quality material in any cycling tests up to 20 cycles





Results – Coupon Sizes





150 mm Low Quality 20 Cycles LN2

25mm - Microcracking visible
75mm - Reduced microcracking potentially due to slower cooling due to increased thermal mass
150mm - Significant microcracking, likely caused by non-uniform cooling







Cooling of 150mm specimens

- Film boiling recedes from edges to centre in a rectangular pattern.
- Indicate in plane cooling faster than through thickness cooling.
- Leads to temperature differential across specimen causing increased stresses.





- Coupons warped after cooling, cracking dominates on one side.
- Could be caused by cooling specimens horizontally.
- Film boiling could be insulating

150mm - non-uniform cooling can cause thermal gradient leading to significant microcracking







Initial Testing Trends

- For the composite materials tested, rate of cooling appears to have more effect on composite microcracking than absolute temperature, however this may vary from material to material.
- Coupon size has an impact on microcracking behavior under rapid cooling, potentially due to increased thermal gradients within the larger coupon.
- Tough materials may not crack under thermal cycling until several hundred cycles. An automated cycling rig has been developed to enable testing of tough materials to higher cycles.
- In addition to thermal cycling, other cryogenic composite characterisation methods are being developed including a "Cryogenic Microcrack Fracture Test" involving combined thermal and mechanical loading. *To be presented later in the year*







Questions?

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