

# **MICROCRACKING OF CFRP COMPOSITES DURING CRYOGENIC THERMAL CYCLING**



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### **Hydrogen as an Alternative Fuel**



Values in brackets account for tank weight assuming composite hydrogen tanks.

**Why Liquid Hydrogen?** Minimised mass and size compared to other alternatives



#### *LH2 Tank Schematic*

**Why Composites?** Literature and modelling predict around 50% weight saving for composite inner skin over a Type I Al-Li baseline. (Vickers, 2013)

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## **Stresses in Cryogenic Composite Tanks**

#### **Thermal Stress**

Coefficient of Thermal Expansion (CTE) is a challenge in composite materials as the constituents can have opposing CTE.

- **Carbon Fibres** Negative CTE axially Elongate on cooling.
- **Polymer Matrices** Positive CTE Contract on cooling.
- **Ply Level** interaction between fibres and matrix.
- **Laminate level** interaction between plys at different angles.

### **Mechanical**

- Internal Pressure in the region of 2-10 bar
- Fluid sloshing during 9g crash case

**Role of constituents in composite LH2 tank**

**Fibres** experience the majority of the mechanical stress from the pressure loading.

**Matrix** experience transverse thermally induced stress from the fibres expanding.

Adding more fibres does not improve performance, it increases the transverse matrix stresses!



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# **Micro-Cracking**

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- Constituents expand and contract relative to each other leading to Internal stresses.
- Polymers become brittle at cryogenic temperatures.
- Material damage occurs through matrix microcracking.

#### **The Microcracking Problem**

A fully linked network of microcracks in a tank will enable permeation of hydrogen

**Any surface microcracks may cause** Pleratures. catastrophic failure if hydrogen becomes trapped during warming







# **Cryogenic Composite Screening Methods**

- **Resistance to cryogenic microcracking** The primary factor for assessing the suitability of composite materials for use in cryogenic tanks.
- **Thermal cycling followed by microcrack inspection**  The most common screening method In literature.
- Thermal Cycling Methods Vary in literature.

### **Cooling fluid**

- $LN<sub>2</sub>$
- LHe •

### **Cooling Method Cooling Method**

- <mark>Immersion</mark>
- **Vapour cooling** •  $\frac{\text{LN}_2}{\text{LHe}}$  •  $\frac{\text{LHe}}{\text{Mmersion}}$  • Ambient<br>• Immersion • Cycle time<br>• Vapour cooling • Heating

### **Heating method**

- **Elevated**
- Ambient Ambient

### **Cycle time**

- Cooling rate
- Heating rate Heating rate

### **Areas Investigated**

### **Cycle temperature temperature**

- Lower temperature
- Upper temperature •

### **Coupon geometry Coupon geometry**

- Shape
- **Size**





# **Cooling Methods**



**Immersion** No cooling rate control – thermal shock Lower temperature fixed to that of the cryogenic fluid

**LN2 Immersion Vapour Dipping** Control of cooling rate and lower temperature



#### **LHe Vapour Dipping**







## **Film Boiling in immersion**





#### **Video of film boiling on coupon**

### **Film Boiling**

Cooling rate influence by film boiling, reduces heat transfer between fluid and object



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**Double Walled Glass Beaker**

• LN2 has faster cooling rate then LHe

**Immersion**



## **Cooling Methods**







# **Specimens**

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- **Plate specimens with two polished edges to inspect for microcracks with optical microscopy**
- **Layup**
	- **16 Ply QI Blocked**
	- $[0_2/45_2/-45_2/90_2]$
- **Sizes**
	- **25 mm x 25 mm**
	- **75 mm x 75 mm**
	- **150 mm x 150 mm**
- **Materials**
	- **Multiple thermoset and thermoplastic materials tested**

![](_page_8_Figure_13.jpeg)

![](_page_8_Picture_14.jpeg)

![](_page_9_Picture_2.jpeg)

### **Two Materials Presented**

**Initial**

![](_page_9_Picture_6.jpeg)

![](_page_9_Picture_7.jpeg)

**Low Quality material** has more porosity / Voids **High Quality material has increased toughening** 

![](_page_9_Picture_10.jpeg)

![](_page_10_Picture_0.jpeg)

![](_page_10_Picture_2.jpeg)

### **Effects of LN2 Immersion – Low Quality Material 25mm**

![](_page_10_Picture_5.jpeg)

microcracking

For testing purposes, a low quality material was made with stress raisers and defects to generate microcracking.

Significant microcracking occurred when cooled rapidly at 15 K/s to 77K.

![](_page_10_Figure_8.jpeg)

![](_page_10_Picture_9.jpeg)

3000

![](_page_11_Picture_2.jpeg)

# **Effects of LHe Cycling – Low Quality Material 25mm**

![](_page_11_Figure_4.jpeg)

In comparison when cooled slowly at 0.5 K/s to 20K reduced microcracking was visible, in some coupons there were no microcracks.

![](_page_11_Figure_6.jpeg)

![](_page_11_Picture_7.jpeg)

![](_page_12_Picture_0.jpeg)

![](_page_12_Picture_2.jpeg)

### **Effects of LN2 Immersion – High Quality Material 25mm**

![](_page_12_Picture_5.jpeg)

No Cracking in high quality material in any cycling tests up to 20 cycles

![](_page_12_Picture_8.jpeg)

![](_page_13_Picture_2.jpeg)

### **Results – Coupon Sizes**

![](_page_13_Figure_4.jpeg)

![](_page_13_Picture_5.jpeg)

![](_page_13_Picture_6.jpeg)

25mm - Microcracking visible

75mm – Reduced microcracking potentially due to slower cooling due to increased thermal mass 150mm – Significant microcracking, likely caused by non-uniform cooling

![](_page_13_Picture_9.jpeg)

![](_page_14_Picture_0.jpeg)

![](_page_14_Picture_2.jpeg)

# **Cooling of 150mm specimens**

- Film boiling recedes from edges to centre in a rectangular pattern.
- Indicate in plane cooling faster than through thickness cooling.
- Leads to temperature differential across specimen causing increased stresses.

![](_page_14_Picture_7.jpeg)

![](_page_14_Picture_8.jpeg)

- Coupons warped after cooling, cracking dominates on one side.
- Could be caused by cooling specimens horizontally.
- Film boiling could be insulating

150mm - non-uniform cooling can cause thermal gradient leading to significant microcracking

![](_page_14_Picture_13.jpeg)

![](_page_15_Picture_0.jpeg)

![](_page_15_Picture_2.jpeg)

# **Initial Testing Trends**

- For the composite materials tested, rate of cooling appears to have more effect on composite microcracking than absolute temperature, however this may vary from material to material.
- Coupon size has an impact on microcracking behavior under rapid cooling, potentially due to increased thermal gradients within the larger coupon.
- Tough materials may not crack under thermal cycling until several hundred cycles. An automated cycling rig has been developed to enable testing of tough materials to higher cycles.
- In addition to thermal cycling, other cryogenic composite characterisation methods are being developed including a "Cryogenic Microcrack Fracture Test" involving combined thermal and mechanical loading. - *To be presented later in the year*

![](_page_15_Picture_8.jpeg)

![](_page_16_Picture_0.jpeg)

![](_page_16_Picture_2.jpeg)

# **Questions?**

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![](_page_16_Picture_6.jpeg)

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