

1 **Biochar production from sewage sludge and microalgae mixtures: properties,**
2 **sustainability and possible role in circular economy**

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16

17 **Abstract**

18 Possible destination for sewage sludge sustainable disposal is its transformation in biochar,
19 achieved by post-processing of the sludge itself through pyrolysis. Biochar from sludge is
20 considered one of the most interesting final products in wastewater-based circular economy, as
21 proven by the multitude of its possible uses tested so far in different areas. Recently, combined
22 activated sludge (AS)-microalgae systems have been proposed to simultaneously remove both
23 carbon and nutrients from wastewaters, as alternative to conventional technologies such as those
24 based on AS. Such innovation could be efficient from the point of view of removal of regulated
25 components from effluents, but it adds potential issues to solid residue disposal practices, as algae
26 normally respond poorly to traditional, mechanical drying processes. In this study, a disposal
27 solution was investigated, consisting of pyrolysis of a mixed sludge/bioalgae matrix under
28 different conditions: in such way, not only landfilled residuals are practically eliminated, but a
29 material with multiple possible beneficial end uses is generated. Initial materials (algae, sludge and

30 combinations thereof) and end-products (biochar and bio-oil) were physically and chemically
31 characterized after pyrolysis under different conditions. Algae alone were also subject to
32 preliminary solvent oil extraction to assess whether increased biochar production would result from
33 this process modification (which did, increasing biochar production by 25-33%). A comprehensive
34 discussion on properties of end products as function of process design, possible applications in a
35 circular economy cycle, and advantages of co-pyrolysis follows.

36

37 **Keywords**

38 Slow pyrolysis – microalgae – *Chlorella* – Biochar analysis – Bio-oil – Sewage sludge disposal

39

40 **Introduction**

41 Increasing industrialization, demographic expansion and expansion of the transportation and
42 mobility sector worldwide, and especially in developing countries, are the cause of excessive
43 conventional fossil fuels exploitation, leading not only to repeated energy shortages worldwide, but
44 also to increasing global levels of greenhouse gases emissions [1]. Renewable feedstocks and
45 energy sources are thus being investigated to face the demand for cleaner energy alternatives, in
46 order to fulfil growing energy demands. Moreover, increasing carbon dioxide and greenhouse gases
47 emissions into the atmosphere have prompted the ethical obligation to investigate more sustainable
48 and environmentally neutral energy sources [2,3]. A current area of intense investigation is the
49 exploitation of biomasses for energy production [4,5]. Amongst them sewage sludge, the final
50 residue of wastewater treatment in the integrated water cycle, is getting increasing attention as not
51 only it normally requires additional expensive treatment and disposal costs by generating utilities,
52 but it is also targeted for sustainable recovery of materials and energy, in compliance with
53 increasingly ambitious EU objectives of generating circular economy cycles from waste streams
54 [6] in accordance to new paradigms in urban water management [7]. Cost of sludge disposal has
55 been estimated at around 50% of the total cost of wastewater treatment [8] while, at the same time,
56 disposal alternatives under current strategies are getting increasingly limited, since accumulation of
57 heavy metals, organic pollutants and pathogenic organisms in the sludge narrow its continued use in
58 commonly adopted practices, such as direct land disposal and composting [9]. Among possible
59 alternatives, incineration would significantly reduce the quantity of waste to be disposed of,
60 allowing energy cogeneration at the same time [10]. However, this involves high costs for effluent
61 gas treatment, which may contain metals, acidic components and dioxins, in addition it generates

62 residual ashes considered hazardous waste. and may be poorly accepted, or outright opposed by
63 public opinion. Therefore, researchers' interest has switched to non-combustion, more
64 environmentally sustainable technologies such as gasification and pyrolysis. Pyrolysis is the
65 thermal degradation of biomass in the absence of oxygen, resulting in the production of liquid (bio-
66 oil) and solid (biochar) residues, and gaseous products (py-gas), effectively transforming wastes
67 into valuable products [11,12,13,14]. These show different possible applications, in particular
68 biochar has proven multiple uses as solid fuel, soil conditioner for agricultural land, and industrial
69 applications in flue gas cleaning, as building material, or aid in contaminated sites remediation [15].
70 Also, high process temperatures, favour increased stabilization of metals, that concentrate in sewage
71 sludge, into the carbonaceous char matrix, considerably reducing the possibility of their release into
72 soil, and ultimately into the food chain [12,16]. Depending on heating velocity and residence time
73 of the process, pyrolysis can be broadly classified as slow (conventional), or fast. Slow pyrolysis
74 maximises solid fraction (biochar) production, and occurs at long residence times and slow heating
75 rates, while liquid and gaseous energy-rich products (bio-oil or py-gas) fractions are increased
76 during fast pyrolysis [17]. An increase of pyrolysis temperature generally maximizes the gaseous
77 fraction, minimizing the solid yield [18]. Properties of the solid residue (biochar) also vary in terms
78 of carbon content and composition. Concerning energetic aspects, bio-oil and biochar could be used
79 as fuels, meeting increasing needs for energy from non-fossil fuels sources [19,20]. However,
80 biochar derived from sewage sludge generally presents high ash content and lower heating value,
81 diminishing its energetic worth [11].

82 For this reason, an interesting opportunity could consist in the application of co-pyrolysis of
83 sludge with microalgae, which have been recently investigated both as a wastewater treatment
84 process and potential energy feedstock [21]. Microalgae are unicellular photosynthetic
85 microorganisms capable of fixing carbon dioxide by photosynthesis, with several characteristics
86 that make them suitable for energy recovery [22]. These include: (i) absence of competition with
87 food supply, (ii) high productivity with reduced cultivation areas (oil yield of about 70% by weight
88 of dried biomass, with area requirement of just 0.1 m²/year per kg extracted), (iii) growth possibility
89 on areas not suitable for other crops, without subtraction of soil from food crops cultivation, (iv)
90 production in most types of water (fresh, brackish and waste water), with minimal or positive
91 impact on water resources use [23]. Microalgae present positive impact also on carbon dioxide
92 emissions, in fact they contain about 50% C over dry weight derived mainly from atmospheric CO₂,
93 therefore, production of 100 tons of microalgae allows fixation of about 183 tons of carbon dioxide
94 [24]. High growth rate, cultivation ease, high lipid and low ash contents makes microalgae highly
95 appealing, compared to other biomasses, with high yields in terms of both bio-oil and biochar [25],

96 as determined with satisfactory results by numerous studies [26–28]. Growth and productivity of
97 microalgae are strongly influenced by environmental and physiological factors, such as
98 temperature, pH, light intensity and nutrient availability [29]. Microalgal biochar has lower carbon
99 content than biochar from other feedstocks, lower surface area, and lower cation exchange capacity,
100 while pH, ash and nitrogen contents and extractable inorganic nutrients are high. These properties
101 make it a useful additive to enhance soils characteristics and improve crop productivity, particularly
102 for acidic soils [12].

103 Recently, combined activated sludge (AS)-microalgae wastewater treatment systems have
104 been proposed to remove simultaneously both carbon and nutrients from liquid streams, as a more
105 energy sustainable and economic alternative to conventional technologies (e.g. AS with nitrification
106 and denitrification). The cultivation of microalgae in wastewater allows direct removal of nitrogen
107 and phosphorus contained within, producing up to 1 kg of dry biomass per m³ of wastewater [30].
108 In this alternative to conventional AS processes, bacteria oxidize the organic substance in
109 wastewater to inorganic compounds consuming oxygen, while microalgae use sunlight to absorb
110 inorganic nutrients released by bacteria, including CO₂, producing oxygen subsequently used by
111 bacteria for oxidation. Although efficient for liquid streams treatment, such systems generate a
112 residue that is more difficult to handle, as algae normally respond poorly to traditional sludge
113 mechanical separation and drying processes. In fact, algal cells are small (2-20 µm), with density
114 similar to that of water, and rather low (0.5-0.3 g L⁻¹) concentration in wastewater [31].
115 Purpose of this paper is to evaluate biochar and bio-oil production through thermal pyrolysis
116 processes starting from these initial residues (microalgae and AS waste sludge) and their
117 combination, and to determine which conditions are more favourable to optimal recovery of
118 valuable by-products.

119

120 **2. Materials and methods**

121 Three different materials were tested, characterized and pyrolyzed at two different
122 temperatures throughout the following experiments. Both initial materials and final products were
123 characterised using thermogravimetric analysis (TGA) and infrared spectroscopy (IR). HHV (higher
124 heating value) in recovered biochar samples was also evaluated.

125 *2.1 Samples preparation*

126 A mixed culture of microalgae *Chlorella* was cultivated in four lab-scale open reactors
127 (0.35·0.20·0.10 cm, constant water depth 3 cm) in BG-11 medium (Table 1)

128 **Table 1.** Chemical composition of the BG-11 medium

Compound	Concentration (mg L ⁻¹)
NaNO ₃	1500
MgSO ₄ ·7H ₂ O	75
K ₂ HPO ₄	40
CaCl ₂ ·2H ₂ O	36
Na ₂ CO ₃	20
Citric acid	6
Ferric ammonium citrate	6
H ₃ BO ₃	2.86
MnCl ₂ ·4H ₂ O	1.81
EDTA (disodium salt)	1
NaMoO ₄ ·2H ₂ O	0.39
ZnSO ₄ ·7H ₂ O	0.222
CuSO ₄ ·5H ₂ O	0.079
Co(NO ₃) ₂ ·6H ₂ O	0.049

129

130 A domestic aquarium aerator provided air bubble agitation to keep microalgae in suspension, light
 131 was provided by a conventional warm light LED bulb (40 W) under a 16:8 light:dark sequence.
 132 Once the culture reached stable growth, microalgae were harvested, dried on nylon filters ($\phi = 0.25$
 133 μm) for 12 h, and pulverized to uniform size in a mortar.

134 Sewage sludge (mixture of primary and secondary sludge) was collected from a nearby wastewater
 135 treatment plant and dried at 100°C for 12 hours (reaching humidity content below 10%).

136 The third material tested was a mixture of sludge and microalgae with high humidity content,
 137 collected from a phytoremediation plant in Spain (kindly supplied by FCC Aqualia S.A.). Fresh
 138 material was distributed in 2 cm layers in a crystallizer, and then dried at 100°C for 12 hours to
 139 reduce humidity below 10%. Subsequently, dried material was shredded, to obtain a resulting grain
 140 size as uniform as possible.

141

142 2.2 Oil extraction from microalgae

143 Previous studies assessed that preliminary oil extraction from dried microalgae samples lead
 144 to enhanced bio-oil and biochar recovery yields from a subsequent thermal processing. Combination
 145 of a two-step lipid extraction and slow pyrolysis processing regime may in fact yield an oil product
 146 high in valuable fatty acids, with no variation on its quality, compared to the one-step process, with
 147 overall increased yields of liquid and solid fractions over the gaseous one [32,33]. Therefore,
 148 preliminary microalgae solvent oil extraction was performed using a chloroform-methanol ratio 2:1,
 149 as described in [29]. From a fraction of the two algae-containing materials described in the previous
 150 section, 1 g of dried sample was immersed in 20 mL of solvent solution in a flat-bottomed pyrex
 151 glass flask, stirred for 25 minutes, then centrifuged for 20 mins at 4000 rpm. The liquid fractions

152 were then filtered and evaporated in a rotary evaporator (Rotovapor, Buchi) to remove solvent and
153 determine the weight of the extracted oil.

154

155 *2.3 Thermogravimetric analysis (TGA) and infrared spectroscopy (IR)*

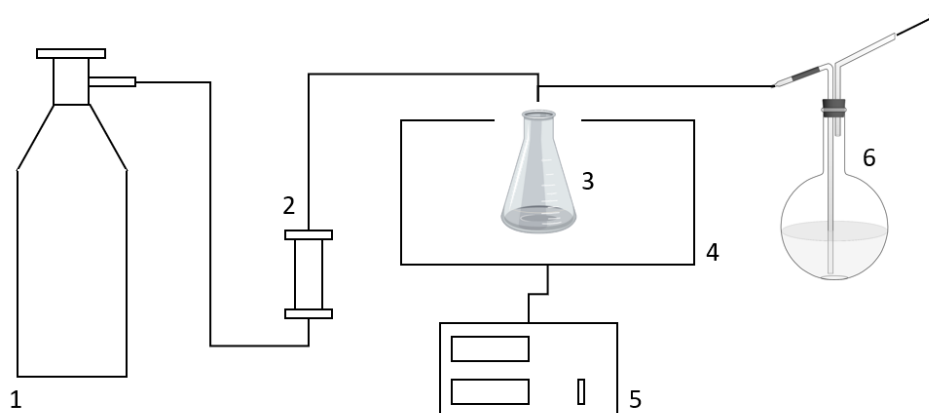
156 Aliquots (20 g each) of the initial and processed materials (sludge, algae and sludge mix,
157 powdered algae) were subject to thermogravimetric analysis (TGA, 25÷800 °C, heating speed 20 °C
158 min⁻¹, with TGA1 Star System, Mettler Toledo). TGA analysis weights any changes in samples as
159 function of increasing temperatures. Thermal degradation of samples occurs in multiple stages
160 between initial and final temperature settings. TGA was first conducted under nitrogen (nitrogen-
161 TGA) atmosphere (0.4 L min⁻¹) to identify the temperature at which pyrolysis process began, later
162 under air (air-TGA), to determine samples' ash and inorganic material content. Both nitrogen- and
163 air-TGAs were subsequently carried out also on solid residue samples deriving from pyrolysis, to
164 assess the characteristics of processed materials, and compare their ash content. Subsequently, a
165 nitrogen-TGA analysis was carried out on residues of microalgae subject to solvent oil extraction.
166 Infrared spectroscopy (IR) was also used to characterize initial materials, liquid and solid residues
167 from pyrolysis, and to detect any presence of water in liquid samples.

168

169 *2.4 Pyrolysis process and products recovery*

170 Initial substrates were pyrolyzed in a thermostatic sand bath S-70 (FALC instruments)
171 during the experiments. Process equipment is schematized in Figure 1. A flat-bottomed pyrex glass
172 flask containing 20 g of sample was immersed within the heating sand medium in contact with its
173 bottom. The absence of oxygen was ensured by continuous flow of nitrogen blown directly inside
174 the reactor. A three-way glass fitting was connected by silicone tubing to a solvent trap containing
175 acetone, and immersed in crushed ice, for recovery of the oily fraction. Py-gas thus flowed through
176 the tubing, entering the trap where it condensed. The non-condensable py-gas was not further
177 characterized and eliminated from the system. Experiments were conducted at 500°C and 350°C
178 temperatures for each sample. In tests at 500 °C the oven was kept operating at maximum
179 temperature, monitoring the temperature curve with a thermocouple inserted in the sand bath. Once
180 the desired set-point was reached, temperature was kept constant for 30 minutes before switching
181 off the heating device. As for the remaining tests, temperature was monitored with the
182 thermocouple until reaching 350°C, manually maintaining this value for about 30 minutes by acting
183 on the oven's thermoregulator. After cooling, the process' solid and liquid products were recovered.

184 All tests were conducted in triplicate. Table 2 summarizes samples analyses throughout the
 185 experiment.



186

187 **Figure 1** – Schematic of the pyrolysis equipment. 1) Carrier gas tank (N₂); 2) flowmeter; 3)
 188 Erlenmeyer flask containing sample; 4) sand bath; 5) thermocouple; 6) scrubber with solvent trap

189

190 **Table 2** – Tests summary

Sample ID	Substrate	Temperature
1	Microalgae <i>Chlorella</i>	500 °C
2	Microalgae <i>Chlorella</i>	350 °C
3	Sludge from WWTP	500 °C
4	Sludge from WWTP	350 °C
5	Mix Algae +Sludge	500 °C
6	Mix Algae+Sludge	350 °C

191

192 Solid (biochar) and liquid (bio-oil) product fractions were recovered from each test, while
 193 the uncondensed gas fraction was considered irrelevant for purposes of this work, and only
 194 estimated through mass balance. After completion of each pyrolysis test, all glassware and tubing
 195 were washed with acetone to remove all residual solid and oil particles still contained therein. This
 196 resulted in a mixture of biochar, bio-oil, acetone and water, subjected to further treatment for
 197 components separation. For the solid fraction, filtration with Buchner funnel, with weigh
 198 determination before and after filtration to quantify the separated fraction was performed. The liquid
 199 fraction (a mixture of acetone and oil) was transferred into a balloon flask, and vacuum evaporated
 200 using Rotavapor R-100 (BUCHI) to remove the solvent, weighting the flask before and after the
 201 process. In case water were detected in the sample during IR analysis, anhydrous Na₂SO₄ was added
 202 to the solution, that was then filtrated and evaporated.

203 Yields of biochar and bio-oil recovered were calculated as follows (Eqs. (1) and (2), respectively):

$$y_{char} = \frac{W_{biochar}}{W_i - W_{H_2O}} \cdot 100 \quad (1)$$

where $W_{biochar}$ is the weight of biochar recovered, W_i is the initial sample weight (20 g) and W_{H_2O} is the water weight in the initial sample, as determined from TGA analysis, and

$$y_{oil} = \frac{W_{bio-oil}}{W_i - W_{H_2O}} \cdot 100 \quad (2)$$

where $W_{bio-oil}$ is the weight of bio-oil recovered, W_i is the initial sample weight (20 g) and W_{H_2O} is the water weight in the initial sample, as before.

210

211 2.5 Biochar thermal properties

212 The calorific value (HHV - higher heating value) of recovered biochar samples was
 213 measured with adiabatic calorimeter IKA C6000 Global Standard, in accordance with UNI EN
 214 14918:2010.

215

216 3. Results

217 3.1 Initial materials characterization

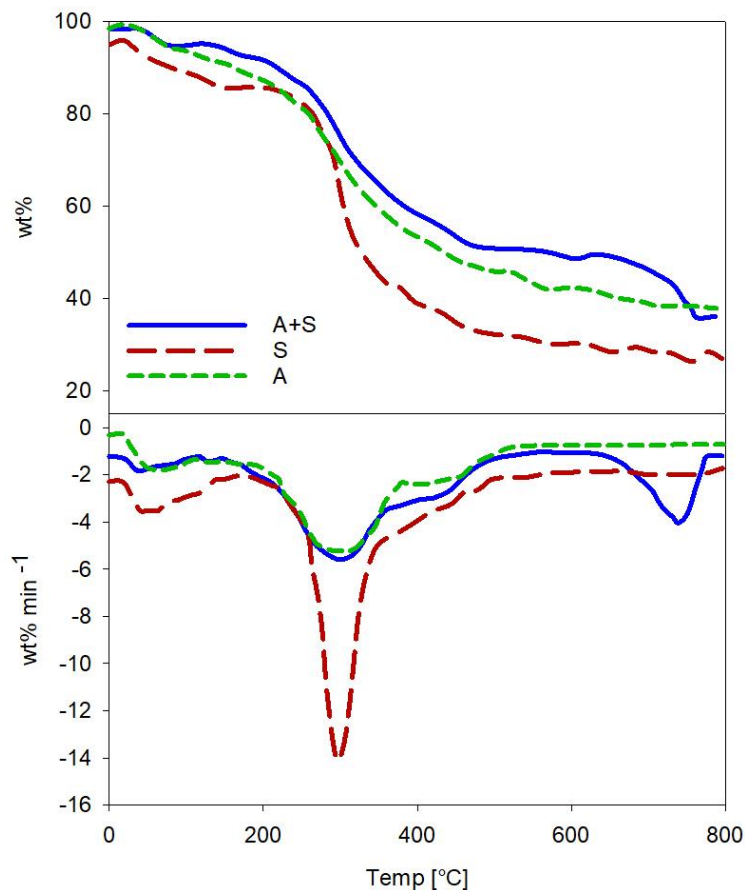
218 TGA was carried out on each initial sample to determine its thermal degradation behaviour.
 219 Each material was characterized by both air-TGA (oxidative environment, reproducing a
 220 combustion process) and nitrogen-TGA (inert environment), between temperatures of 25 - 800°C.
 221 An oxidative environment allows the ash content of the tested material to be evaluated. TGA in
 222 inert atmosphere was also needed to determine the temperature range suitable to pyrolyzation of the
 223 samples being tested. The thermochemical process in absence of oxygen leads to degradation of
 224 volatile substances in the sample, leaving char as residue. Results of the TGA in both air and
 225 nitrogen are summarized in Table 3. According to derivative thermogravimetry (DGT) analyses,
 226 thermal degradation of microalgae takes place in one single stage, as reported in previous studies
 227 [34], while that of mixed sludge and algal samples occurs in two distinct phases. It should be
 228 highlighted that the temperature range 200-500°C includes the highest degradation peaks for all
 229 samples (Figure 2). These are generally associated with carbohydrate and protein de-volatilization
 230 [35]. In mixed samples a second peak between 600-700°C also appears, corresponding to
 231 degradation of lipids and solid residues [36].

232 **Table 3** – Amount of ashes (%) in the three samples based on TGA analyses.

Substrate	% ashes (800 °C)	% residues (char+ashes, 800°C)
Microalgae <i>Chlorella</i>	13.7 ± 2.6	25.1 ± 1.4
Sludge WWTP	30.2 ± 1.8	36.2 ± 2.1
Mix A+S	24.4 ± 3.1	38.7 ± 1.9

233

234 Based on ash fractions obtained from TGA analyses, composition of mixed microalgae and
 235 sludge from the phytoremediation plant sample was confirmed as 15% and 85% of each,
 236 respectively. Ash content in WWTP sludge sample was higher ($30.2 \pm 1.8\%$) than in those
 237 containing microalgae, meaning that adding even a small amount (15%) of microalgae to the mix
 238 positively contributes to the reduction of the ash quantity in residues, improving their energy
 239 quality. As for nitrogen-TGA results, it is relevant to see that the quantity of solid residues from the
 240 sludge-microalgae mix, is higher than that produced by the single-sludge matrix, leading to
 241 increased yield in solid material recovery.



242

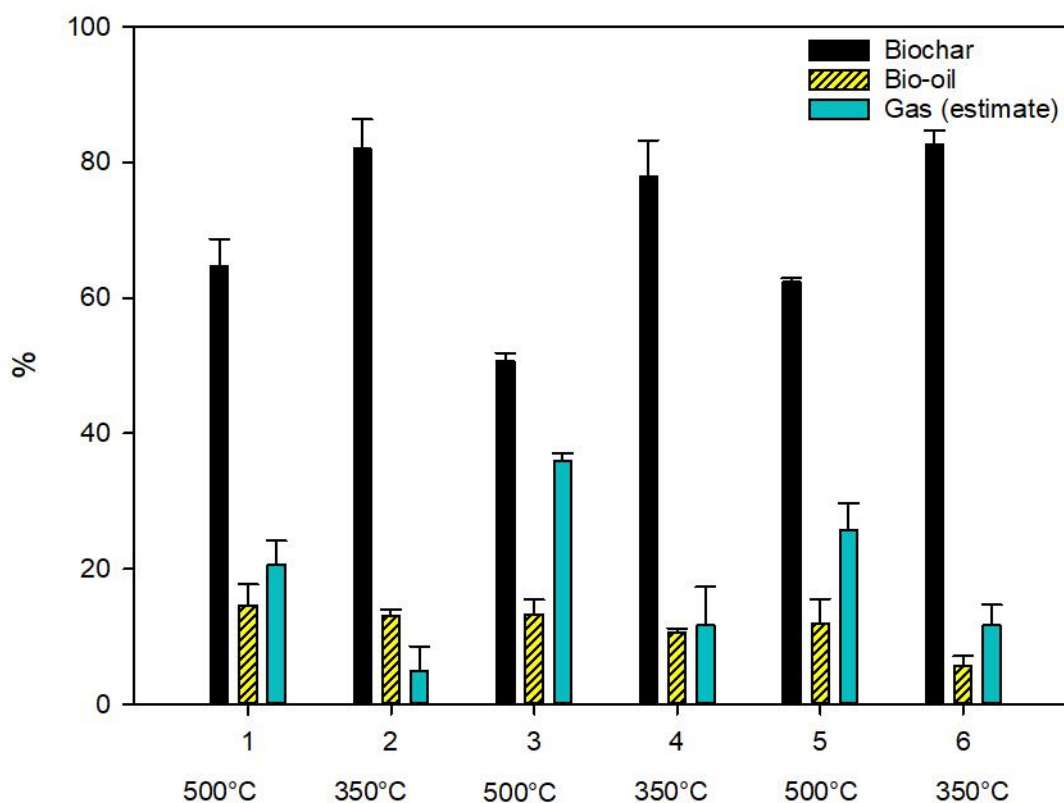
243 **Figure 2** – TG and DTG thermograms of the initial materials
 244 (microalgae (A), sludge (S), and mix microalgae and sludge (A+S))
 245

246

247 3.2 Biochar production and characterization

248 Resulting pyrolysis products from tests at 350°C and 500°C were solid (biochar) and liquid
249 (bio-oil) residues. After recovering and separating solid and liquid particles remained in the testing
250 equipment, biochar was weighed directly.

251 Figure 3 represents the product fractions obtained from tests. For all matrixes examined, pyrolysis
252 at 350°C produced the greatest amount of solid residue (biochar), while higher temperatures (500
253 °C) generally yielded higher production of bio-oil. Considering only the production yield of
254 biochar, WWTP sludge processed at 350°C gave higher values ($82.0 \pm 4.4\%$) along with the mixed
255 sample at the same temperature ($82.7 \pm 2.1\%$). As for liquid residues (bio-oil) yields, higher
256 temperatures usually originate higher fractions than those obtained in the present work [37],
257 nevertheless, all samples processed at 500°C produced $13 \pm 3\%$ of bio-oil, a fraction higher than at
258 lower temperature.

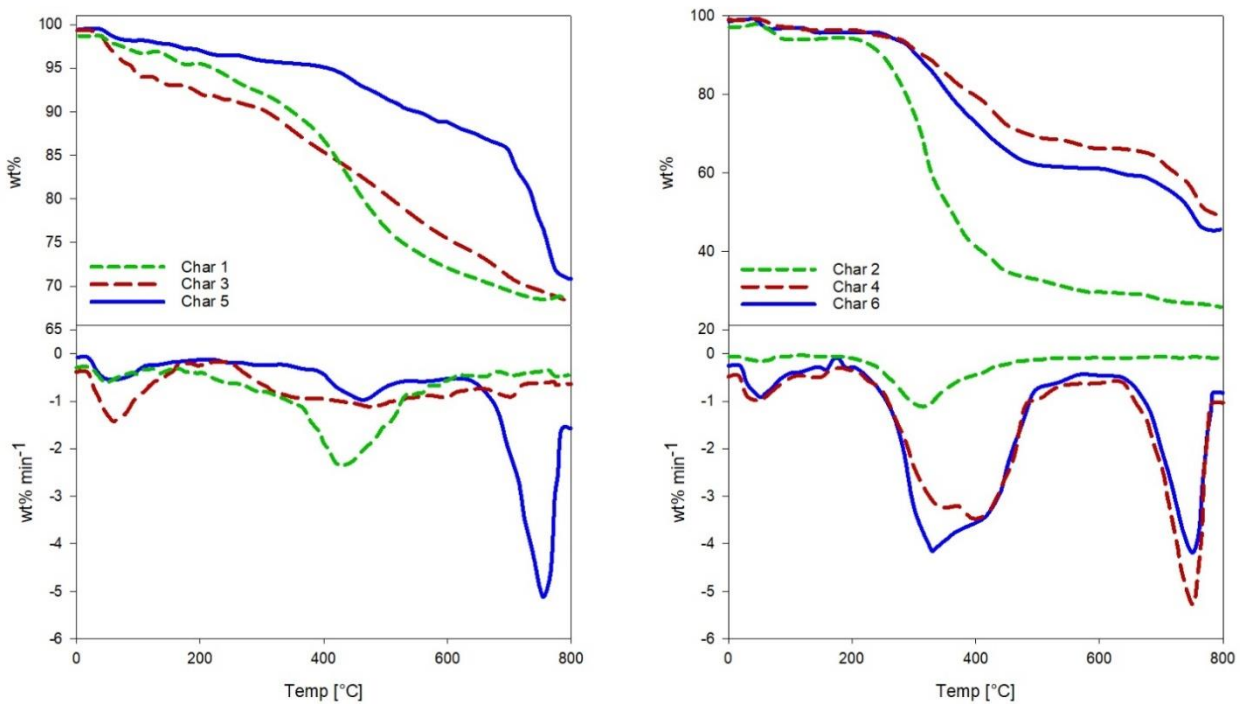


259

260 **Figure 3** – Pyrolysis products: biochar (black), bio-oil (yellow) and gas (light blue, estimated).
261 Error bars represent variability of results between triplicates

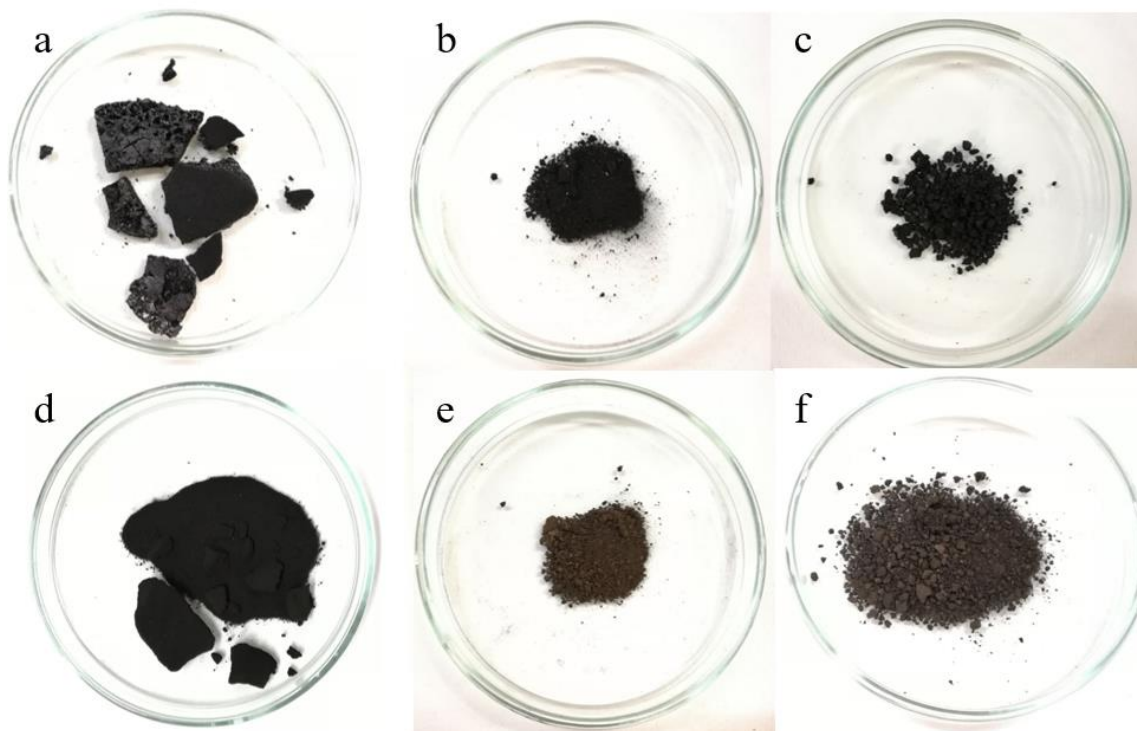
262

263 Due to the focus of the present work, only the solid residue was fully characterized. Biochar
264 samples from pyrolysis tests were subject to TGA, IR analysis and HHV (High Heating Value, UNI
265 EN 14918:2010). Under visual analysis, all samples appeared different from each other, with
266 appearance changing according to process temperature and initial material. Samples 2 and 4 from
267 tests at 350°C (Figure 5 e, f) presented fairer color (brownish), compared to all others (black or
268 blackish). Among microalgae-derived biochar samples 1 and 2 (Figure 5 a, d, respectively) no
269 colour differences were detected, but they significantly differed in consistence: sample 2 (Figure 5
270 d) had a dusty structure, while sample 1 was mostly solid (Figure 5 a). Air-TGA analyses were
271 performed to evaluate ash content of the biochar samples, while nitrogen-TGA was used to evaluate
272 the efficiency of the pyrolysis process (Figure 4), by assessing their supplemental weight loss.



273

274 **Figure 4** – TGA and DTG thermograms of biochars from pyrolysis at different temperatures.
275 Left: 500°C; right: 350°C. Heating speed constant for all processes (20°C min⁻¹).

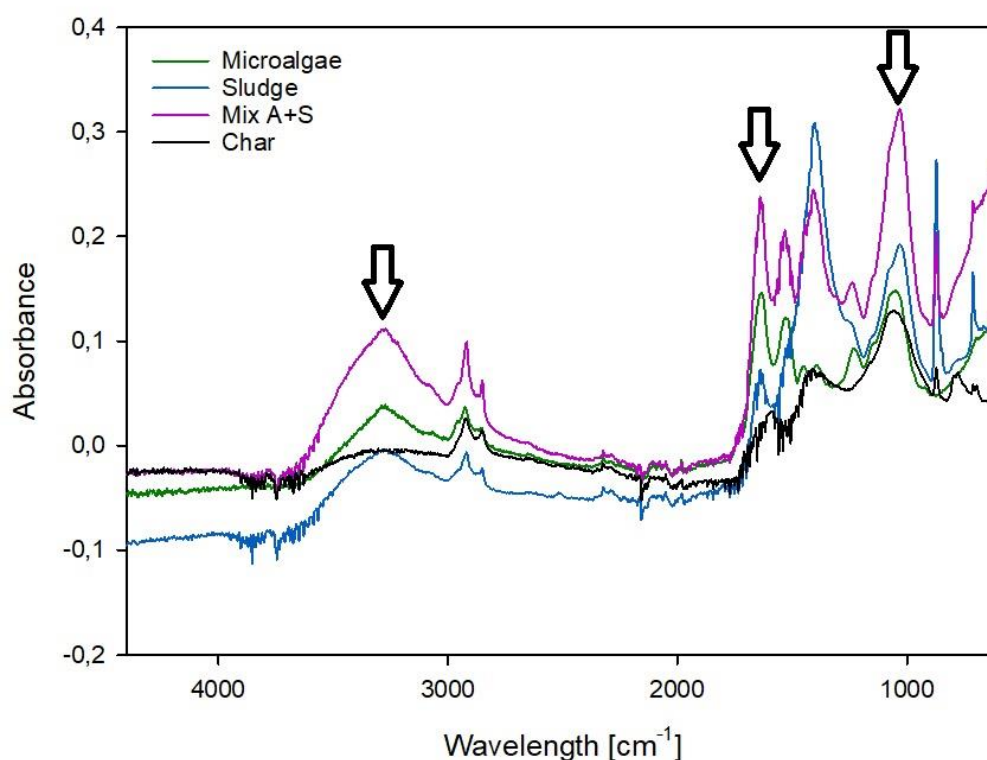


276

277 **Figure 5** – Upper: samples from pyrolysis at 500°C a) microalgae *Chlorella*; b) sludge from
 278 WWTP; c) Mix M+S. Lower: samples from pyrolysis at 350°C: d) microalgae *Chlorella*; e) sludge
 279 from WWTP; f) Mix M+S.

280

281 IR analysis was performed before and after pyrolysis to evaluate variation of internal
 282 material bonds induced by the process (Figure 6), by determining functional groups and bonds
 283 within samples. The most significant information in the graphs are contained in the wavelengths
 284 representing water and carboxyl groups (between 3600-2500 cm^{-1}), C-C and C-H bonds (3300 cm^{-1});
 285 esters and fatty acids (1700 cm^{-1}), and Si-O bonds in inorganic material (1100 cm^{-1}). By
 286 comparing the different spectra, all samples before pyrolysis appear very similar to each other,
 287 although some relationships between components vary. Pyrolyzed samples (only one sample is
 288 reported in the figure) show removal of water and organic acids during the process, and reduction of
 289 many of the functional groups present. This corresponds to formation of compounds with high
 290 carbon content, even if some C-C and C-H bonds are still present. Obviously, Si-O bonds are
 291 preserved, as not involved in pyrolysis reactions. Further increasing time of pyrolysis process and
 292 temperature would lead to formation of a graphitic carbon, with absence of IR bands detected.



293

294 **Figure 6** – IR analyses results. Absorbance curves for initial materials and for biochar from Mix
 295 A+S at 350°C are shown. Arrows show the relevant sections.

296

297 HHV analysis shows that microalgae-derived biochar has higher heating value (samples 1
 298 and 2) than others, decreasing with decreasing process temperature. HHVs of remaining samples,
 299 are lower, suggesting that thermal uses might not be indicated as the main final application of these
 300 biochars. Significant results are summarized in Table 4.

301

302 **Table 4** – Amount of ashes detected by air-TGA, weight loss (incomplete pyrolysis) from nitrogen-
 303 TGA analysis, and HHV value of biochars obtained in tests (1-6).

Sample	Pyrolysis temperature [°C]	Ashes [%]	Weight loss [%]	HHV [kJ kg ⁻¹]
1	500	41.6 ± 2.3	16.8	29091
2	350	31.5 ± 1.7	67.5	26951
3	500	50.1 ± 2.2	23.9	16629
4	350	37.0 ± 1.9	46.2	15648
5	500	44.3 ± 2.7	26.8	16245
6	350	34.5 ± 3.0	49.3	16671

304

305 To assess the effect of solvent oil pre-extraction from microalgae on biochar production
 306 yield, as suggested in previous studies [32, 33], solid residues after this pretreatment were subject to

307 nitrogen-TGA, comparing the results with those on raw materials. These samples showed
308 significantly better results, than initial ones: biochar production yield after pre-extraction increased
309 from 25% to 33% in microalgae-only samples. However, no benefits were detected from such
310 preliminary oil extraction in the mixed samples (microalgae and sludge), with 38% biochar yield in
311 both cases.

312

313 **4. Discussion**

314 This work aimed to assess potential advantages in terms of biochar production and
315 characteristics of the combination of sewage sludge and microalgae as feedstock in pyrolysis
316 processes, with a view to improve the final use value of recovered resources. Product analysis was
317 not limited at observing mass weight obtainable from each matrix, but was extended to determine
318 ash fractions in the final products, and their quality. Alternatives for coupling the two matrixes in
319 one feedstock are feasible: one option could consist of separate microalgae production with direct
320 addition to sludge at the time of pyrolysis. However, this strategy would be of small benefit
321 compared to the direct use of a microalgae-sludge mix originated by a wastewater treatment facility
322 of new conception. This novel type of process, in fact, in addition to allowing simultaneous
323 nutrients removal from wastewater by microalgae, without costly bio-denitrification processes,
324 produces a mixed biomass (sludge and microalgae), originating a solid residue with excellent
325 characteristics after thermal treatment, as reported.

326 *4.1 Comparative analysis*

327 Observed product yields were compared with those obtained by other authors, to validate
328 present results (Table 5). Sewage sludge biochar was obtained by slow pyrolysis in helium
329 atmosphere using a quartz tubular reactor containing 30 g sludge samples by Sanchez et al. [38]. In
330 this study the original matrix had ash content of 3.4% by weight. Tests were conducted at 350, 450,
331 550 and 950°C, with the largest amount of biochar (52%) produced at the lower temperature of 350
332 °C, in accordance with the present study.

333 Microalgae-derived biochar was obtained by Gong et al. [35] using a quartz, fixed-bed reactor
334 under inert (N₂) gas flow, testing 1 g samples at temperatures between 300 and 700°C, with heating
335 rate of 10°C min⁻¹. The study showed that bio-oil fraction increased with temperature from 30.9%
336 (at 300°C) to a maximum of 60.7% (at 500°C), decreasing afterwards to 48.1% (at 700°C). As for
337 biochar yield, the highest amount was obtained at 300°C (57%), decreasing with temperature to a
338 minimum of 25.5%. HHV of the char also decreased with temperature (from 22.3 to 16.4 MJ kg⁻¹),

339 while gas yield increased along with temperature (from 0.4 to 15.5%). Compared to the results of
 340 this study, char production yield from the *Chlorella* culture was higher, as well as the product HHV.
 341 Results from microalgae and sewage sludge mixtures in this study could not be compared due to the
 342 lack of similar literature data concerning these feedstocks co-pyrolysis. The highest productions of
 343 biochar were detected in pyrolysis of microalgae alone, while intermediate results were obtained
 344 from co-pyrolysis of sewage sludge and microalgae, as expected by preliminary information
 345 reported in other studies on co-pyrolysis of microalgae with other, non-sludge matrixes [12].

346

347 **Table 5** – Product yields of microalgae and sewage sludge pyrolysis.

Feedstock [Reference]	Pyrolysis type	Temperature [°C]	% biochar	% bio-oil	% gas	HHV [MJ kg ⁻¹]
Sewage sludge [38]	Slow	350	52	10	20	-
Sewage sludge (this study)	Slow	350	74.3	11.5	14.2	15.6
<i>C. vulgaris</i> [34]	Slow	500	31.5	49.2	4.6	19.3
<i>C. vulgaris</i> [36]	Fast	500	34.0	41.5	24.5	-
<i>C. vulgaris</i> residues [39]	Fast	500	31.0	53.0	11.0	19.4
<i>Chlorella</i> (this study)	Slow	350	78.9	6.0	15.1*	26.9
<i>Chlorella</i> (this study)	Slow	500	58.8	10.2	31.0*	29.1

348 * gas value estimated

349

350 4.2 Possible beneficial applications of biochar

351 Pyrolysis operating conditions are paramount to determine optimal final uses of derived
 352 biochar, since these factors directly contribute to the development of different intrinsic
 353 characteristics of the product [40]. It is therefore important to analyse feedstock materials before
 354 thermal processing, in order to establish *a priori* the best application for the biochar that will be
 355 obtained under given operating conditions. Results obtained in this study from HHV analysis on
 356 obtained biochars, compared with HHV of hard coal (around 30 MJ / kg), prove that biochar from
 357 microalgae could in fact be used as fuel (HHVs of 29.1 and 26.9 MJ/kg, not dissimilar from coal's
 358 value). As biochar is the product of renewable feedstock, this would substitute the caloric
 359 equivalent amount of fossil fuels, offsetting related GHG emissions. However, other alternative
 360 uses of this product are known, a more interesting one being its use in agriculture as soil
 361 enhancement or in wastewater or contaminated site remediation as pollutants adsorbent, either a use
 362 with greater added value compared to outright combustion. Agricultural use will effectively work as
 363 long-term carbon sequestration (also valuable under current policies), uses as adsorbent will
 364 substitute other commercial products, after which the spent biochar could be sent to controlled
 365 combustion, that would simultaneously serve as final contaminants destruction and exploitation of
 366 the char energy content.

367 The most interesting outcomes for these products, regardless of original feedstock, are in
368 fact considered to be those related to the possibilities of their re-use and valorisation, from an urban
369 (wastewater) based circular economy perspective. An appealing use of biochar is that of soil
370 improver in agriculture, that has shown to allow increase in crop productivity, but also to reduce
371 soil pollution by adsorbing metals and other solute contaminants in groundwater [41]. Biochar in
372 fact has excellent adsorbent capacities for both organic and inorganic pollutants, and by virtue of its
373 C content, also acts as a long-term carbon sink. For proper agricultural use, biochar carbon content
374 must be greater than 50% (dry mass), N and P content should be between 1 and 45%, pH should not
375 exceed 10, and particles' specific surface should be greater than $150 \text{ m}^2\text{g}^{-1}$ [42, 43]. Biochars
376 derived from bagasse and vegetal biomass feedstocks generally fit these specifications, and some
377 studies confirmed that also microalgal biochar presented compatible characteristics [44, 45]. Effects
378 of biochar on physical-chemical improvement of soils also depend strongly on the original soil
379 characteristics and on feedstock used for its production [46].

380 A recent study from Oliveira and co-workers [47] showed that low pyrolysis temperatures
381 ($<500^\circ\text{C}$) favour partial carbonization, producing biochar with smaller pores and reduced surface
382 area, while increasing the presence of oxygen-containing functional groups, making it ideally
383 suitable for removal of inorganic pollutants. On the contrary, biochar produced at high temperatures
384 ($> 500^\circ\text{C}$) could be applied for adsorption of organics, due to higher specific surface area, making it
385 highly suitable for environmental bioremediation of organic pollution and for wastewater treatment
386 applications, specifically for removal of toxic compounds, instead of activated carbon (AC) [48]. In
387 that respect, Alhashimi and Aktas [49] performed a LCA (life cycle assessment) analysis evaluating
388 the relative economic and environmental performance of biochar as adsorbent, compared to AC.
389 Environmental impact was evaluated in terms of energy demand and GWP (Global Warming
390 Potential) for their production. GWP of biochar generation is usually negative ($-0.9 \text{ kgCO}_{2\text{eq}} \text{ kg}^{-1}$),
391 against an average $6.6 \text{ kgCO}_{2\text{eq}} \text{ kg}^{-1}$ of commonly used AC. Energy demand for biochar production
392 is lower than that required for AC by one order of magnitude ($1.1 \div 16 \text{ MJ kg}^{-1}$ for biochar, $44 \div$
393 170 MJ kg^{-1} for activated carbon). However, it has to be considered that spent AC is usually not
394 discarded immediately, but regenerated for reuse, while spent biochar is usually destroyed after its
395 first use. As for economic aspects, biochar and AC industrial production costs are comparable,
396 estimated as $\$5 \text{ kg}^{-1}$ and $\$5.6 \text{ kg}^{-1}$, but this does not factor in the missed high costs for the original
397 sewage sludge disposal that would otherwise be needed. Some drawbacks of biochar as adsorbent
398 must also be considered, such as less controllable quality and fluctuating efficiency, longer time
399 needed for absorption of certain contaminants, differences in performance of products from
400 different feedstocks. However, environmental advantages are obvious and with adequate

401 optimization biochar may be considered suitable for most adsorption applications. Finally, due to its
402 high carbon content, biochar has found other applications, for example for use as electrode material
403 in bioelectrochemical systems (BES) in lieu of granular graphite or AC, and many others [42].

404

405 *4.3 Implications for a biochar-based Circular Economy*

406 All the above mentioned and other additional applications of biochar will gradually be
407 investigated and validated as circular economy becomes an effective part of new economic
408 paradigms. In order to encourage the development of a biochar-based circular economy, attempts at
409 certification of biochar are being carried out. Biochar at the moment is defined according to
410 guidelines from the International Biochar Initiative (IBI Biochar Standards) [50] and the European
411 Biochar Foundation [51]. The former concerns the use of biochar uses in soil, the latter consists of
412 guidelines for sustainable production of biochar. Both these guidelines define biochar as material
413 produced by pyrolysis of biomass under low oxygen conditions, without limitations to the origin of
414 the biomass, therefore both sewage sludge and algae fall under this definition. Both guidelines
415 include specifications about maximum toxicants assessment, and their maximum allowed
416 thresholds. Product certification, although at present existing only for a restricted range of
417 applications, is an important step for setting up reliable and lasting circular economy circuits. While
418 circular economy strategies centered on wastewater treatment by-products in the EU generally
419 postulate their direct re-use in energy production, and alternative could be based on their
420 transformation into new products, not necessarily limited to agricultural use. In order to fulfil future
421 certification and regulation requirements for these products, the next challenge for research and
422 development of biochar-based products lies in achieving a greater understanding and control of
423 pyrolysis processes starting with feedstock pretreatment, additives addition, effect of process
424 operating parameters, process yield in terms of specific product properties, such as heavy metal
425 immobilization, specific surface area, elemental analysis, phosphorus and micropollutants contents.

426 Decentralized biochar production units would constitute the most efficient way to meet
427 local by-products demand with specific characteristics by using homogeneous site-produced
428 feedstock under purpose-designed process conditions, avoiding the economic and environmental
429 impacts of long-range transportation, promoting local business and employment and locally
430 improving resource efficiency and synergistic opportunities for various local sectors in the
431 transition to circular economy paradigms.

432

433 **5. Conclusions**

434 This study aimed at assessing the effects of adopting mixtures of sewage sludge and
435 microalgae as feedstock in terms of these residuals' pyrolysis disposal processes, and specifically of
436 possible improvements of biochar production quantity and quality. Final product analysis was not
437 limited at the determination of relative mass produced from each matrix, but also went further to
438 determine the ash fractions, carbon and energy properties of each final product. Results showed that
439 slow pyrolysis of mixed feedstock (85 and 15% sludge and algae respectively) at temperature of
440 350°C, yielded 80% of the initial sample by weight as biochar, of which only 24% as ash.
441 Comparing this result to the data from pyrolysis of WWTP sludge at the same temperature, biochar
442 extracted was 74% of the initial sample weight, but with 30% ash content. Therefore, co-pyrolysis
443 of sewage sludge and microalgae yielded a more valuable product, with multiple possible
444 applications. This solution could contribute to the reduction of problems deriving from expensive
445 and/or inappropriate disposal of wastewater treatment residuals.

446 Various possibilities in terms of implementation of productive biochar reuse have been
447 described. Within a wastewater-based circular economy cycle, biochar is a very valuable material,
448 with multiple possible interesting outlets that need further careful evaluation beyond currently
449 known applications. Standardization and certification of final products characteristics are the keys
450 to a successful circular economy implementation. Some attempts in this sense have been already
451 developed for specific biochar applications. Decentralization of biochar production from local
452 feedstock sources would be the most logical and effective way to implement efficient biochar-based
453 circular economy. Such systems would benefit from more homogeneous feedstock characteristics
454 and the possibility to custom-define and design the required final products characteristics according
455 to local applications, and minimize additional environmental impact.

456

457

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461

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