

1 **Thermoanalytical study of the decomposition of yttrium trifluoroacetate thin films**

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13 **Abstract**

14 We present the first use of the thermal analysis techniques to study yttrium trifluoroacetate thin
15 films decomposition. In situ analysis was done by means of thermogravimetry, differential
16 thermal analysis, and evolved gas analysis. Solid residues at different stages and the final product
17 have been characterized by X-ray diffraction and scanning electron microscopy. The thermal
18 decomposition of yttrium trifluoroacetate thin films results in the formation of yttria and presents
19 the same succession of intermediates than powder's decomposition, however, yttria and all
20 intermediates but YF_3 appear at significantly lower temperatures. We also observe a dependence
21 on the water partial pressure that was not observed in the decomposition of yttrium
22 trifluoroacetate powders. Finally, a dependence on the substrate chemical composition is
23 discerned.

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26 **Keywords:** thermal analysis, thin films, yttrium trifluoroacetate, yttria, thermal decomposition.
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1 **1. Introduction**

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3 Among the different routes described for the synthesis of $\text{YBa}_2\text{Cu}_3\text{O}_{7-\delta}$ (YBCO)
4 superconductors, Chemical Solution Deposition (CSD) methods are especially suited for
5 practical purposes since they are flexible, low-cost and scalable [1,2]. In particular, since their
6 early discovery by Gupta et al [3], metal trifluoroacetates (TFA) have been extensively used in
7 the synthesis of high performance YBCO superconducting films [4-9]. CSD involves solution
8 preparation, solution deposition and a temperature thermal treatment to remove the organic
9 species and to crystallize the amorphous films.

10 Thermal analysis (TA) techniques are routinely used to characterize the thermal
11 decomposition of precursors. TA analysis allows us to monitor the evolution of the
12 decomposition under different temperature programs and atmospheres. TA analysis combined
13 with structural characterization provides useful information about the decomposition mechanism
14 as well as its dependence on the treatment conditions [10-15]. Although CSD is used to
15 synthesize thin films, TA studies are customarily carried on powders. The main reason is that the
16 signal in TA measurements is proportional to the sample mass, and thin film masses are at least
17 one order of magnitude smaller than the usual masses of powders. Recent studies have shown
18 that the actual behavior on thin films may significantly differ from that observed on powders
19 [16-19]. The reason is that the transport mechanisms involved on the solid-gas reaction that
20 govern the decomposition process are enhanced on thin films due to the large surface to volume
21 ratio.

22 The aim of this paper is to analyze the thermal decomposition of Yttrium trifluoroacetate
23 ($\text{Y}(\text{TFA})_3$) in the form of films, under different conditions of atmosphere, thickness and
24 substrate. $\text{Y}(\text{TFA})_3$, combined with barium and copper TFAs, is the most common precursor in
25 the fabrication of high-performance YBCO superconducting tapes [4,5,9]. Thermogravimetry
26 (TG), differential thermal analysis (DTA), and differential scanning calorimetry (DSC) are used
27 to monitor the decomposition process. The volatiles formed during decomposition are analyzed
28 using evolved gas analysis (EGA) performed with a mass spectrometer (MS). Final and
29 intermediate products are characterized using scanning electron microscopy (SEM) and X-ray
30 diffraction (XRD). We focus our attention on the differences with respect the behavior reported
31 for powders [20,21]. In particular, we observe that films decomposition starts at a lower

1 temperature than powders. Contrarily to powders, the decomposition depends on the water
2 partial pressure and no combustion is observed in films. Finally, decomposition is enhanced for
3 substrates with cation terminations.

4 5 **2. Experimental**

6 *2.1 Chemicals*

7 Anhydrous Y(TFA)₃ with a purity of 99.99% (trace metals basis) was supplied by Aldrich. A
8 solution 0.66 M of Y(TFA)₃ in methyl alcohol was obtained at room temperature by manually
9 shaking the mixture for less than 1 minute. Films were prepared by freely spreading microdrops
10 (~3 μL) on the surface of a glass disc (12 mm in diameter) or on a square LaAlO₃ (LAO) plate
11 (5×5 or 10×10 mm²). The solvent was removed by heating the substrate at 70°C for 15 minutes
12 in a hot plate under vacuum (pressure around 440 mbar). Nominal film thicknesses were of the
13 order of several hundred nanometers. Nominal thicknesses have been calculated by assuming
14 that the density of pyrolyzed films is that of bulk yttria (5.01 g/cm³), Y₂O₃.

15 16 *2.2 Characterization techniques*

17 TG and DTA analysis was performed with a Setaram apparatus model, Setsys Evolution
18 16. To improve the signal-noise ratio, two substrates coated on both sides were analyzed
19 simultaneously. After the experiments, TG and DTA curves were corrected by subtracting a
20 consecutive identical second measurement and by measuring the sample mass at room
21 temperature after the experiment. Gas flow was controlled by mass flow meters. High purity
22 gases at a flow rate around 50 ml/min were used to control the furnace atmosphere. Water-
23 saturated gases were obtained by bubbling the carrier gas in water at standard temperature and
24 pressure (25°C, 1 atm). Residual oxygen and water partial pressures on the furnace were 0.01%
25 and 0.002%, respectively. EGA analyses were performed by placing the samples inside a quartz
26 tube at a pressure of around 10⁻⁶ mbar. Samples were heated using an external furnace. DSC was
27 performed in a Mettler Toledo DSC model DSC821 with films deposited on a square LAO plate
28 (5x5 mm²) substrate. Thermal analysis experiments were performed at heating rates of 5, 10 and
29 20 K/min.

30 XRD experiments were done in a thin film diffractometer PANalytical model X'Pert PRO
31 MRD. The X-ray beam wavelength was 1.5418 Å (Cu-Kα). SEM observations were performed

1 in a Zeiss DSM 960A scanning electron microscope operated at 20 kV. Samples were coated
2 with a thin film of gold to remove electrostatic charges.

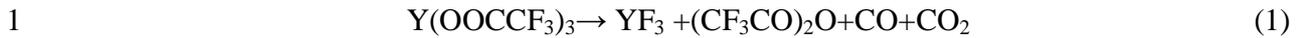
3 4 **3. Results and discussion**

5 Figure 1 shows the TG curves of $Y(TFA)_3$ thin films in LAO substrates heated at 20 K/min,
6 either in wet or in dry atmospheres, with different oxygen partial pressures, and for similar
7 nominal film thicknesses (around 0.4 μm). In Fig 1 the measured mass is normalized to the mass
8 after dehydration. As a reference the expected masses of intermediate and final products are
9 plotted as dashed lines. To facilitate the comparison between powders and films, the
10 decomposition of $Y(TFA)_3$ in the form of powders has also been included in Fig. 1.

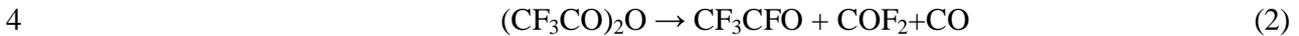
11 The overall precursor decomposition can be divided in four stages, labeled as (I) to (IV).
12 The first stage ends at 150°C and corresponds to the dehydration. Dehydration of anhydrous
13 $Y(TFA)_3$ is related to the water uptake at room temperature of $Y(TFA)_3$ due to its high
14 hygroscopicity [22]. Stages (II) to (IV) involve the formation of intermediates YF_3 , $Y_6O_5F_8$,
15 YOF and the final product Y_2O_3 . Intermediates and final product have been identified by XRD,
16 Fig 2. Precisely, after stage II at 450°C only YF_3 is identified. Above 500°C, YF_3 decomposes to
17 form $Y_6O_5F_8$ and YOF, at 650°C no YF_3 is detected, instead $Y_6O_5F_8$ and YOF are identified and
18 at 730°C traces of $Y_6O_5F_8$, YOF and Y_2O_3 are observed. Finally, YOF decomposes to form
19 Y_2O_3 , at 950°C only Y_2O_3 is observed. In Fig 1 we have plotted (horizontal dashed lines) the
20 expected masses for the formation of YF_3 (34.1%), $Y_6O_5F_8$ (29.8%), YOF (29.0%) and Y_2O_3
21 (26.4%). From, Fig. 1, one can observe that at the end of each stage, the mass of the solid
22 residues coincides with the expected masses of the intermediates and final products. This
23 sequence of intermediates coincides with those reported in powders [21].

24 25 *3.1 Decomposition of $Y(TFA)_3$, stage II.*

26
27 Stage II is the main decomposition step; involves the larger mass loss and results in the
28 formation of YF_3 . The formation of YF_3 is due to the high electronegativity of fluorine which
29 displaces the oxygen bonded to Y [5]. From the EGA analysis in vacuum, Fig. 3, one can
30 observe that the main volatiles formed during stage (II) coincide with those reported for powders
31 [20,21]; namely CO, CO₂ and $(CF_3CO)_2O$:



2 the presence of $(CF_3CO)_2O$ is identified through the fragments $[CF_3]^+$ and $[CF_3CO]^+$. Moreover,
3 in the absence of water $(CF_3CO)_2O$ decomposes to form CF_3CFO , COF_2 and CO :



5 The latter reaction accounts for the larger amount of CO when compared to CO_2 and the
6 presence of fragments $[CFO]^+$, $[CF]^+$ and $[CF_2O]^+$ in Fig. 3 [21].

7 Simultaneous TG-DTA, Fig. 4, confirms that the decomposition is an exothermic process.
8 The enthalpy, measured by DSC, is -220 ± 50 J/g and is in agreement with the enthalpy
9 measured in powders in inert atmosphere [21]. Thus from XRD, EGA and DSC we conclude that
10 the decomposition mechanism is the same in powders than in films.

11 The enthalpy measured in powders was sensitive to the atmosphere; in the presence of
12 oxygen the enthalpy was larger and the DTA peak was not correlated to the mass loss rate signal.
13 This extra contribution in the presence of oxygen is related to the combustion of CO released in
14 reaction (1). This combustion heats the solid sample, but takes place in the gas phase, i.e., it does
15 not affect the mass of the solid residue, thus DTA and TG signals are not correlated. In the case
16 of films, no dependence of the enthalpy on the oxygen partial pressure is observed and the DTA
17 and mass loss rate signals are always correlated, see Fig. 4. This result indicates that there is no
18 effect related to the CO combustion in films. In films, the large surface to volume ration
19 enhances CO removal when compared to the powders, where gas stagnation occurs inside the
20 crucible and in the voids between particles.

21 The enhanced removal of gaseous reaction products in reactions (1) and (2) is also
22 responsible for the lower temperature onset of the $Y(TFA)_3$ decomposition (in powders gas
23 stagnation may significantly slow down the reaction kinetics [23]). Indeed, in the case of
24 powders, after dehydration, the mass remains constant for a temperature interval of around $150^\circ C$
25 before the decomposition onset (Fig. 1), while in the case of films, the mass continues to
26 decrease after dehydration but at a lower rate, i.e., dehydration and decomposition processes
27 overlap. Despite the fact that films start to decompose at a lower temperature, $Y(TFA)_3$
28 decomposition is completed first in powders than in films (see. Fig. 1). The reason is that in
29 powders the low thermal diffusivity of the material and the exothermic nature of the reaction
30 results in a thermal runaway that builds up a fast propagation combustion front. The very abrupt
31 mass loss (Fig 1) as well as the sharp DTA peak (Fig 6 in ref. [21]) observed in powders are

1 typical features of the formation of a combustion front. In the case of films, heat removal is
2 clearly enhanced and combustion is prevented. As a result, the mass evolution is smoother, the
3 mass loss rate, lower, and decomposition is completed at a higher temperature. Numerical
4 integration of the heat propagation in $Y(TFA)_3$ powders and films confirms, respectively, the
5 presence and absence of a combustion front [19].

6 Previous results in powders [20,21] indicate that precursor decomposition does not
7 depend on the oxygen and water partial pressures. This result is in agreement with the fact that
8 neither oxygen nor water are involved in reaction (1). From the inset of Fig. 1, one can confirm
9 that $Y(TFA)_3$ decomposition in films does not depend on oxygen partial pressure but does
10 depend on water partial pressure. Actually, from the inset in Fig. 1, one can observe that at the
11 early stages, decomposition is enhanced in the presence of water. This dependence on the water
12 partial pressure was not observed in powders due to their significantly longer diffusion path. To
13 highlight the effect of water diffusion, in Fig 5 we have plotted the evolution of the
14 decomposition of $Y(TFA)_3$ in wet conditions for different film thicknesses; the thicker the film,
15 the higher the decomposition temperature, thus the lower the water contribution. This
16 dependence on the film thickness is not observed in dry atmospheres.

17 In Fig 6 we have plotted the evolution of $Y(TFA)_3$ decomposition in films deposited over
18 LAO and glass substrates. From Fig 6, one can state that decomposition is enhanced in the case
19 glass substrates. To disclose the effect of the chemical properties of the substrate surface, we
20 have analyzed the decomposition of $Y(TFA)_3$ under the same conditions but with two glass
21 substrates submitted to an acid and basic chemical etching respectively, see Fig. 6 (Chemical
22 etching: room temperature, 0.1 M NaOH and 0.1 M HCl solutions). When compared to the basic
23 etching, the acid etching clearly shifts the decomposition to lower temperatures. Thus, the cation
24 and H^+ terminations of the bare glass and acid etched glass substrates enhances the
25 decomposition $Y(TFA)_3$. Consequently, the decomposition enhancement observed in the
26 presence of water is also related to the presence of H^+ . Since EGA analysis does not reveal any
27 effect on the gas evolved composition due to water, the presence of water does not modify the
28 decomposition mechanism, reaction (1). Actually, it is very reasonable to assume that the
29 presence of cations weakens the bond between Y^+ and the TFA^- groups, as a result, the
30 decomposition takes place at lower temperature.

1 The fact that water diminishes the precursor stability together with the slow water
2 diffusion provides an explanation to the fact that no stable anhydrous intermediate is formed
3 during $Y(TFA)_3$ hydrate decomposition [20] and the impossibility to obtain anhydrous $Y(TFA)_3$
4 by means of a thermal treatment (precursor decomposition starts before the complete removal of
5 water [22]). $Y(TFA)_3$ is very hygroscopic and takes up water very easily when exposed to
6 ambient conditions. Therefore, thermal dehydration is also observed in anhydrous $Y(TFA)_3$, even
7 if they are exposed to ambient conditions for a short time. However, in this case, during the
8 thermal treatment a stable anhydrous intermediate is formed after dehydration [21]. During
9 dehydration, $Y(TFA)_3$ hydrate releases approximately 3.7 water molecules per yttrium atom
10 [20,22], while anhydrous $Y(TFA)_3$ releases 3.0 water molecules per yttrium atom [21]. This
11 extra amount of water present in $Y(TFA)_3$ hydrate is probably responsible for the lower stability
12 of this precursor. Moreover, long time exposure of anhydrous $Y(TFA)_3$ to ambient conditions
13 may result in a significant water uptake that could affect the precursor stability. It is well-known
14 that a large water content in YBCO TFA precursors has a harmful effect on the final properties
15 of the YBCO films [24]. The lower stability of $Y(TFA)_3$ in the presence of water may help to
16 disclose the detrimental effect of the initial water content in the precursor.

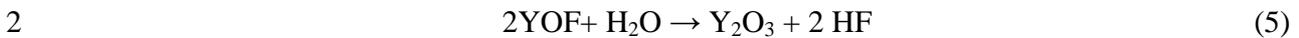
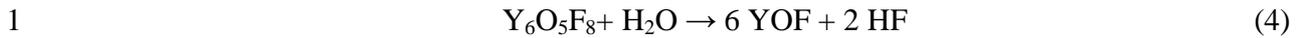
17

18 *3.1 Decomposition of YF_3 and formation of Y_2O_3 stages III and IV.*

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20 From Figs 1 and 2 one can observe that YF_3 decomposes to form non-stoichiometric yttrium
21 oxyfluoride $Y_6O_5F_8$, stoichiometric YOF and finally yttria Y_2O_3 . Compared to the decomposition
22 of $Y(TFA)_3$, the decomposition rate of YF_3 is much slower, it covers a temperature interval
23 larger than 600°C. Noteworthy is the fact all intermediates and yttria are formed at significantly
24 lower temperatures in films than in powders (see Fig 1), e.g., in wet air the transformation of
25 $Y(TFA)_3$ into yttria is completed at 950°C in films and at 1200°C in powders. This result
26 indicates that the reaction is probably controlled by diffusion of a volatile reactive or product.
27 From Fig 1 one can observe that the decomposition is clearly enhanced in the presence of water
28 while no significant dependence on the $P(O_2)$ is observed. Besides, it has been reported that
29 fluorides decomposition is controlled by HF diffusion [5,25,26], therefore we propose the
30 following three step decomposition route:





3 To confirm that reactions (3) to (5) are controlled by diffusion, in the inset of Fig 5, we have
4 plotted the evolution of YF_3 for three films of different thicknesses. One can verify that for
5 reactions (3) to (5), the thicker the film, the higher the decomposition temperature.

6 When compared to powders, the temperature decomposition onset in films shifts down
7 about 250°C. This result indicates that gas transport and renewal is a critical parameter in the
8 decomposition of YF_3 and that in the case of solid gas reactions the decomposition temperatures
9 observed in powders strongly differ from the actual decomposition temperature in films.
10 Although YF_3 decomposes at a significantly lower temperature in films, its decomposition is still
11 too high to understand the YBCO formation. It has been proposed [3,7] that after precursor
12 decomposition, a barium yttrium fluoride is formed that will decompose at a much lower
13 temperature allowing the formation of YBCO.

14

15 SEM analysis, Fig. 7, shows that Y_2O_3 films have a similar morphology than powders
16 [21]. It consists in a granular structure of sintered spherical particles. The size of particles is
17 about 150 nm. Film porosity is very high, as a result, the actual thicknesses are about two times
18 the nominal ones. For instance, in Fig. 7.b the calculated nominal thickness is approximately 1
19 μm while the film thickness is about 2 μm .

20

21 **4. Conclusions**

22

23 We have studied the thermal decomposition of yttrium trifluoroacetate films under
24 different atmospheres. Thermal analysis of films reveals the effect of gas transport on the
25 decomposition behavior, a key aspect of the solid-gas reactions involved in precursor
26 decomposition. For instance, when compared to powders, the larger area to volume ratio
27 significantly enhances gas exchange and diffusion. As a result, films start to decompose at lower
28 temperatures. In particular, all decomposition steps appear at lower temperatures in films than in
29 powders. This decomposition enhancement results in the formation of yttria in films at 950°C,
30 i.e., 250° below the yttria formation temperature reported in powders.

1 The larger area to volume ratio significantly enhances heat transport from the sample to
2 the substrate. Accordingly, during $Y(TFA)_3$ decomposition combustion is prevented. Thus, the
3 decomposition rate of $Y(TFA)_3$ to form YF_3 is much slower in films than in powders.

4 We have observed that the presence of cations weakens the bond between Y^+ and TFA^-
5 groups. Therefore, films start to decompose at a lower temperature in the presence of water or
6 when they are deposited over substrates with positive ions terminations at their surfaces. In
7 addition, a large initial water content in films or powders reduces the precursor stability.

8 The decomposition of YF_3 is controlled by HF out-diffusion. Therefore, gas flow, film
9 thickness and water partial pressure are key parameters to control the decomposition kinetics of
10 YF_3 .

11 To sum up, when analyzing solid-gas reactions, the results obtained from powders cannot
12 be extrapolated to films. Besides, thermal analysis on films provides useful information to
13 disclose the reaction mechanisms and to reveal the effect of gas and heat transport on the
14 decomposition behavior.

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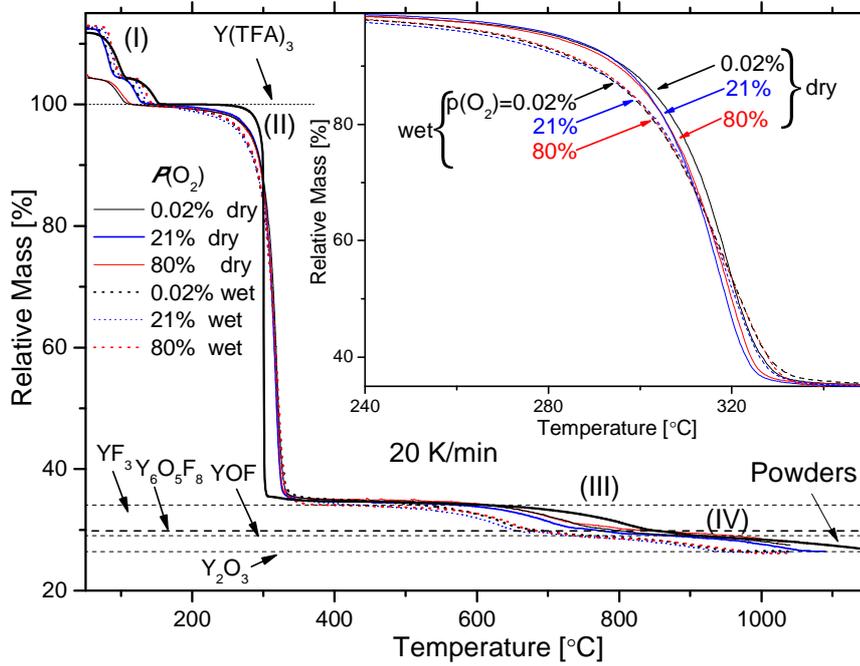
1 $(\text{H}_2\text{O})_{1-x} \cdot \text{THF}$ and $[\text{Y}_4(\mu_3\text{-OH})_4(\mu, \eta^1: \eta^1\text{-TFA})_6(\eta^1\text{-TFA})(\eta^2\text{-TFA})\text{-}(\text{THF})_3(\text{DMSO})(\text{H}_2\text{O})] \cdot 6\text{THF}$
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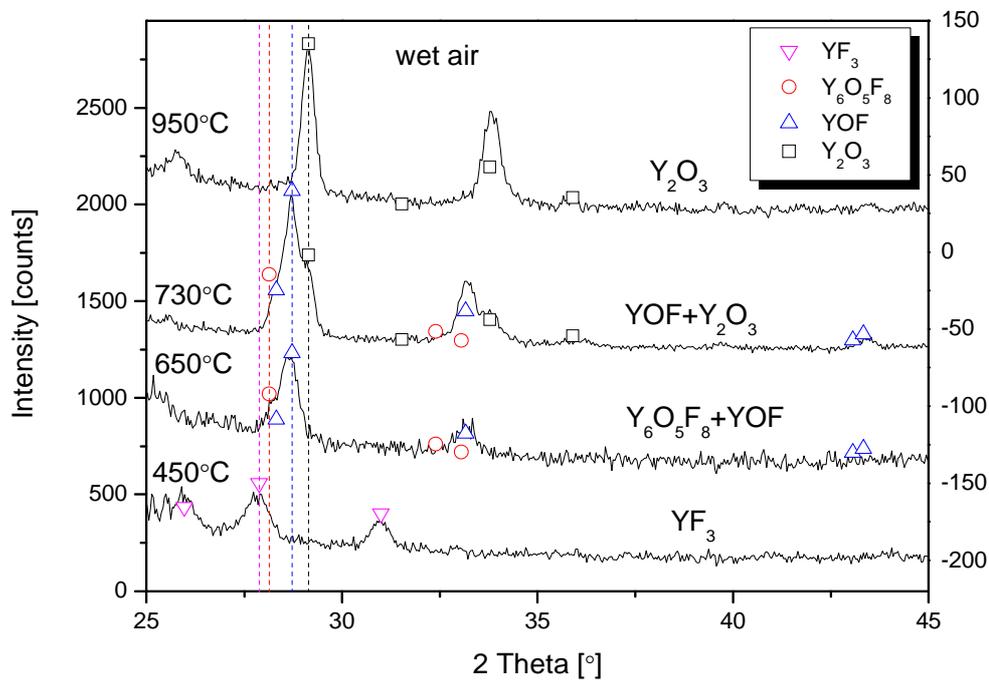
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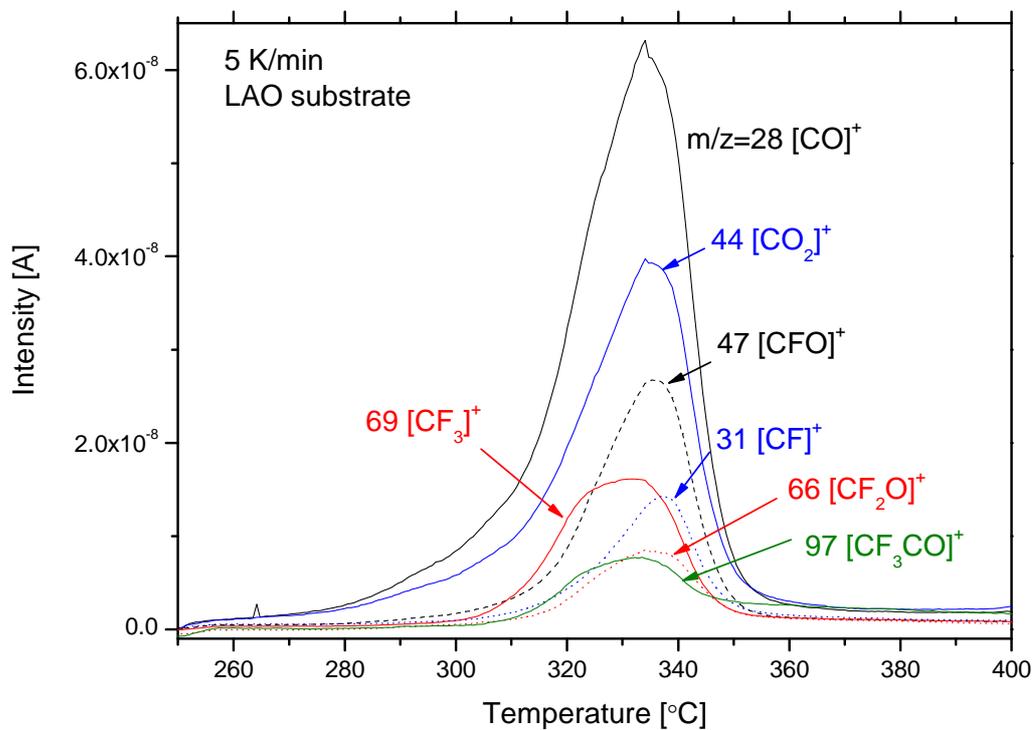


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 2 **Figure 1.** TG curves for thermal decomposition of $Y(TFA)_3$ films, deposited over LAO
 3 substrates, in wet and dry atmospheres with different oxygen partial pressures: air, nitrogen and
 4 oxygen mixture and argon and powders in wet air. Nominal film thicknesses are around between
 5 $0.4 \mu\text{m}$. The initial mass of powders was 10.47 mg. The mass has been normalized to the mass
 6 after dehydration. Inset: detail of the precursor film decomposition for wet and dry atmospheres.
 7 *Horizontal dashed lines:* expected masses for the formation of final and intermediate products.

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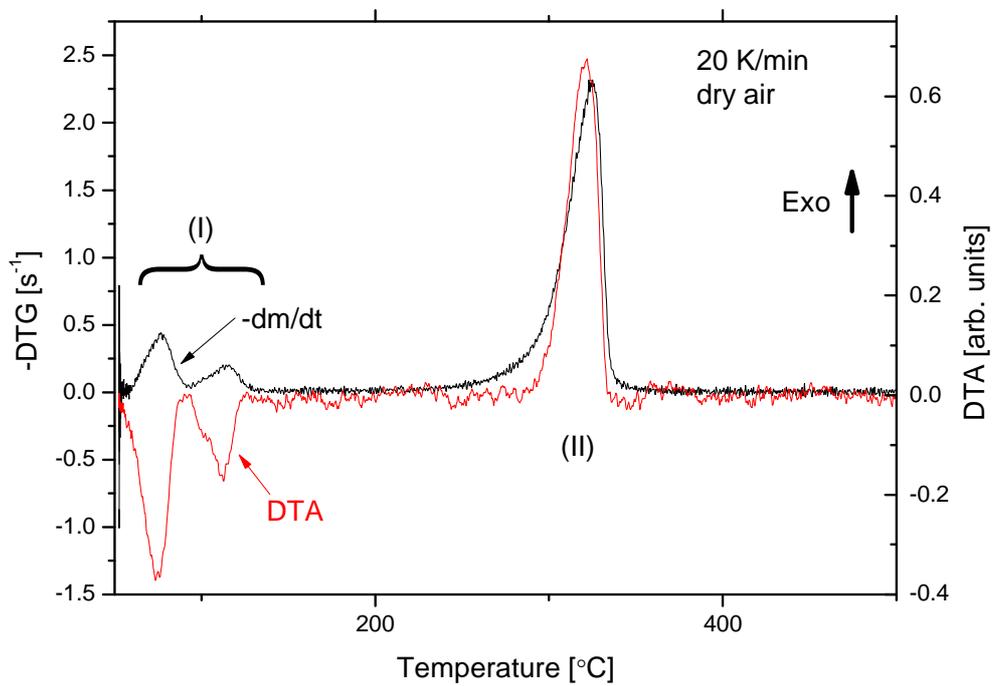


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 2 **Figure 2.** X-ray curves of the Y(TFA)₃ films, deposited over LAO substrates and heated at 20
 3 K/min up to several temperatures.
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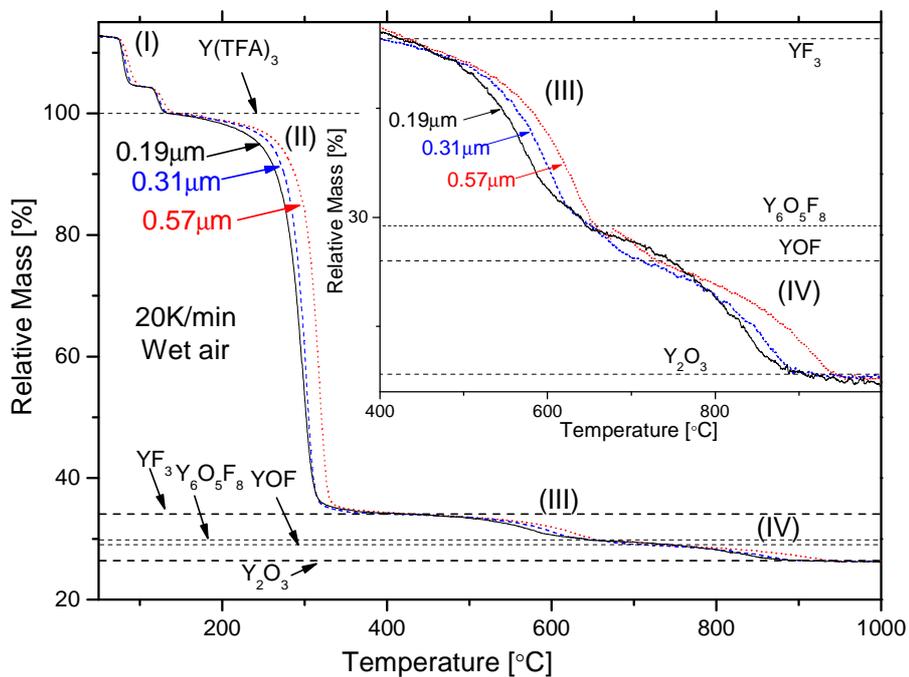
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3 **Figure. 3.** EGA analysis of thermal decomposition of Y(TFA)₃ in vacuum (10⁻⁶ mbar) for a film
4 deposited on a LAO substrate of nominal thickness 0.95 μm. Heating rate is 5 K/min. Only the
5 more intense ions have been plotted.

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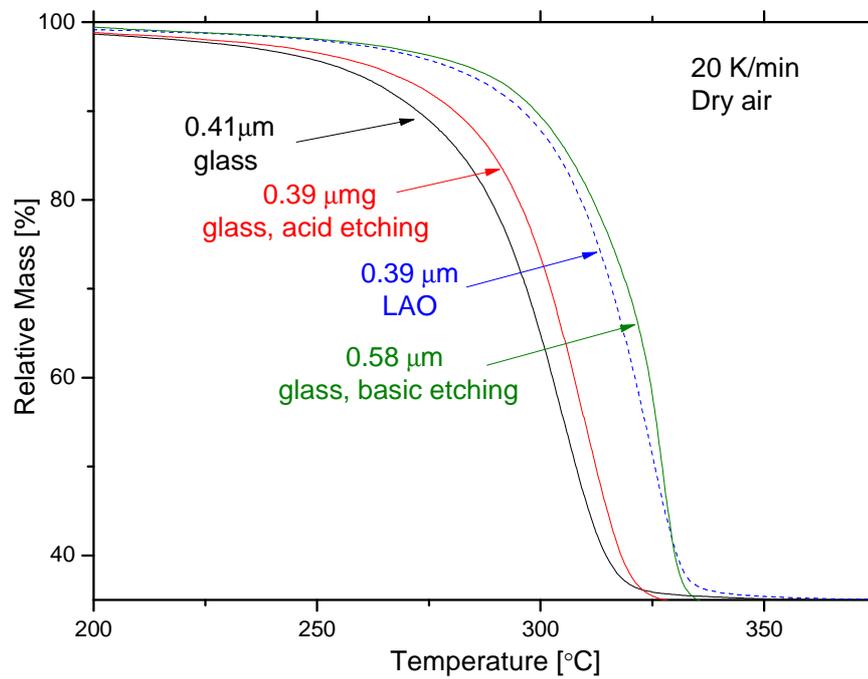
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 2 **Figure 4.** Simultaneous TG-DTA analysis of thermal decomposition of $\text{Y}(\text{TFA})_3$ films,
 3 deposited over LAO substrates, in dry synthetic air ($P(\text{O}_2) = 21\%$). Heating rate is 20 K/min and
 4 the nominal film thickness is $0.39 \mu\text{m}$.

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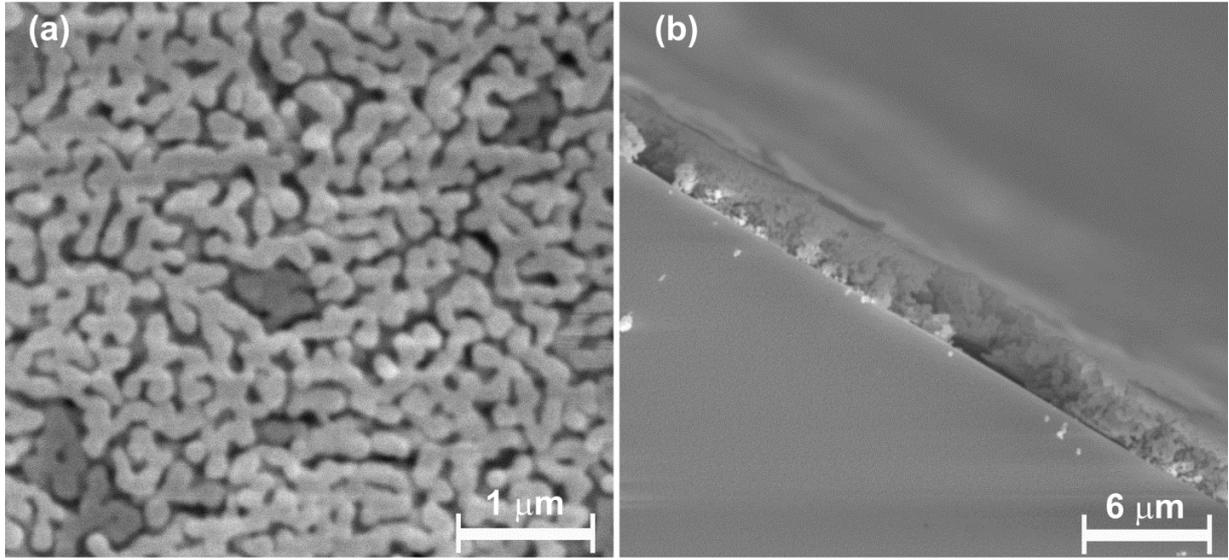


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 2 **Figure 5.** TG curves for thermal decomposition of $Y(TFA)_3$ of films, deposited over LAO
 3 substrates, of different thicknesses heated at 20 K/min in wet synthetic air ($P(O_2)=21\%$). Inset:
 4 detail of last stages of film decomposition.

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2 **Figure 6.** TG curves for thermal decomposition of $Y(TFA)_3$ of films, deposited over different
3 substrates, heated at 20 K/min in dry synthetic air ($P(O_2)=21\%$).
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Figure 7. Scanning electron micrograph obtained when $Y(TFA)_3$ is heated to 950°C at a constant rate of 20 K/min in wet air (a) top view (b) cross-sectional view. The nominal film thicknesses is $0.91\ \mu\text{m}$