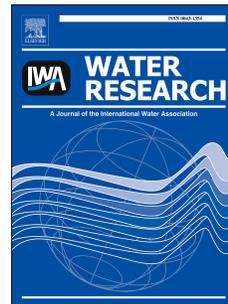


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The Difference Between Energy Consumption and Energy Cost: Modelling Energy Tariff Structures for Water Resource Recovery Facilities

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18

19 **ABSTRACT**

20 The objective of this paper is to demonstrate the importance of incorporating more  
21 realistic energy cost models (based on current energy tariff structures) into existing  
22 water resource recovery facilities (WRRFs) process models when evaluating  
23 technologies and cost-saving control strategies. In this paper, we first introduce a  
24 systematic framework to model energy usage at WRRFs and a generalized structure to

25 describe energy tariffs including the most common billing terms. Secondly, this paper  
26 introduces a detailed energy cost model based on a Spanish energy tariff structure  
27 coupled with a WRRF process model to evaluate several control strategies and  
28 provide insights into the selection of the contracted power structure. The results for a  
29 1-year evaluation on a 115,000 population-equivalent WRRF showed monthly cost  
30 differences ranging from 7 to 30% when comparing the detailed energy cost model to  
31 an average energy price. The evaluation of different aeration control strategies also  
32 showed that using average energy prices and neglecting energy tariff structures may  
33 lead to biased conclusions when selecting operating strategies or comparing  
34 technologies or equipment. The proposed framework demonstrated that for cost  
35 minimization, control strategies should be paired with a specific optimal contracted  
36 power. Hence, the design of operational and control strategies must take into account  
37 the local energy tariff.

38

### 39 **HIGHLIGHTS**

- 40 - A framework to model energy tariff structures was proposed
- 41 - 7-30% difference was obtained when comparing TOU structure vs average  
42 energy price
- 43 - The framework was applied to compare aeration control strategies
- 44 - Proper selection of contracted power resulted in savings without investment

45

46 **KEYWORDS:** wastewater treatment; process control; energy costs; energy tariff;  
47 time-of-use; power demand; benchmark simulation model (BSM).

48

49

50 **ABBREVIATIONS**

- 51 Aerobic tank (AER)
- 52 Benchmark simulation model (BSM)
- 53 Contracted power capacity ( $PC_{P_i}$ )
- 54 Dissolved Oxygen (DO)
- 55 Energy usage charges term ( $EUC_{term}$ )
- 56 Energy consumption per tariff period ( $EC_{P_i}$ )
- 57 Energy usage charge per tariff period ( $r_{VE,P_i}$ )
- 58 External recirculation flow-rate ( $Q_{ras}$ )
- 59 Fixed power charges term ( $FPC_{term}$ )
- 60 Greenhouse gas (GHG)
- 61 High season charges (H)
- 62 Internal recirculation flow-rate ( $Q_{intr}$ )
- 63 Kilowatt (kW)
- 64 Kilowatt hour (kWh)
- 65 Low season charges (L)
- 66 Moderate season charges (M)
- 67 National value-added tax (VAT)
- 68 Peak power demand charges term ( $PDC_{term}$ )
- 69 Peak power demand charges factor rate ( $K_{P_i}$ )
- 70 Proportional-integral controller (PI)
- 71 Proportional-integral-derivative controller (PID)
- 72 Population equivalent (PE)
- 73 Power demand measured ( $PD_{P_i}$ )
- 74 Tariff period ( $P_i$ )

- 75 Taxation term ( $T_{\text{term}}$ )  
76 Time-of-Use (TOU)  
77 Total ammonia ( $\text{NH}_x$ )  
78 Total energy cost (TEC)  
79 Total nitrogen (TN)  
80 Total number of tariff periods ( $P_n$ )  
81 Very low season charges (VL)  
82 Wastage sludge flow rate ( $Q_w$ )  
83 Wastewater resource recovery facility (WWRF)

84

## 85 **1. INTRODUCTION**

86 The high interdependency between water and energy systems, population growth,  
87 climate change, urbanization, increasing living standards and food consumption  
88 requires a holistic evaluation and an integrated approach (Olsson, 2012a). As a result,  
89 efficient and sustainable management of water and energy systems have become a  
90 priority. Within this context, water and energy pricing structures (also called demand  
91 side management or demand response mechanisms) become crucial tools to control  
92 consumption and give incentives to customers to become efficient in the use of water  
93 and energy (Olsson, 2012a).

94 With regards to energy use, energy systems are sensitive to energy consumption  
95 spikes and therefore measures have to be taken either to optimize energy generation  
96 and distribution or better to reduce or shift peak power demands. While there is plenty  
97 of experience in optimizing energy generation and distribution, it is the demand side  
98 that is receiving increasing attention by research and industry (Palensky & Dietrich,  
99 2011). Energy tariff structures are common demand-side management mechanisms  
100 used to improve the energy system in terms of consumption through the application of

101 different energy pricing structures (e.g. time-of-use rates) and charges (e.g. energy  
102 usage, peak power demand charges) in the different billing terms. Those mechanisms  
103 incentivize the reduction or shift of peak power demands at specific times for a  
104 specific duration, avoiding investments in additional infrastructures by balancing  
105 energy use and, consequently, reducing greenhouse gas (GHG) emissions. As an  
106 example, the impact of such tariff structures in the Pennsylvania-New Jersey-  
107 Maryland Interconnection Regional Transmission authority (serving 60 million  
108 customers) was estimated by Spees and Lave (2006). The study concludes that even  
109 small shifts in peak demand would have a large effect on savings to consumers and  
110 avoided costs for additional peak capacity: a 1% shift in peak power demand would  
111 result in savings of 3.9% (billions of dollars at the system level). Such large  
112 reductions would be achieved after encouraging customers and industries to properly  
113 adjust their energy consumption and reduce peak power demands.

114 Water resource recovery facilities (WRRFs) were formerly referred to as wastewater  
115 treatment plants when they largely addressed waste disposal problems while their role  
116 as sources of energy and materials to be mined had not yet been fully recognised.  
117 WRRFs are large energy consumers, albeit minor societal contributors to the  
118 environmental footprint when compared to other manufacturing or human activity  
119 (Olsson, 2012a). Approximately 2-3% of the world's electrical energy is used for  
120 water supply and sanitation purposes, and 1-18% of the electrical energy in urban  
121 areas is used to treat and transport water and wastewater (Olsson, 2012a). The energy  
122 consumption of resource recovery ranges from 335 MWh.month<sup>-1</sup> (WRRFs serving  
123 100,000 population-equivalent or PE) up to 6,600 MWh.month<sup>-1</sup> (WRRFs serving  
124 3,000,000 PE), while the associated energy costs can range from 45,000 €.month<sup>-1</sup> to  
125 280,000 €.month<sup>-1</sup>, respectively. Hence, WRRFs are suitable candidates for the

126 implementation of measures to reduce peak power demand, contributing in this way  
127 to grid stability, decreased energy generation costs and reduced CO<sub>2</sub> emissions.  
128 WRRFs would also benefit monetarily, since their energy bill would be significantly  
129 reduced.

130 Several potential measures can be applied to reduce or shift the power demand of  
131 WRRFs. Flow and load equalization was evaluated as a strategy to shift power  
132 demand by Leu et al. (2009) for a case study in California. Their results showed  
133 decreased costs and even reduction of CO<sub>2</sub> emissions at the energy generation side.  
134 Another possible measure is aeration control, since aeration supply in WRRFs  
135 represents between 50 and 70% of process energy consumption (Reardon, 1995;  
136 Rosso and Stenstrom, 2005; WEF, 2009). Control of aeration has been successfully  
137 brought into practice with reductions in energy consumption as high as 30% (Olsson,  
138 2012b; Amand et al., 2013). These reductions have been converted into monetary  
139 units by using an average energy price (*inter alia*, Cadet et al., 2004; Ekman et al.,  
140 2006; Samuelsson et al., 2007; Stare et al., 2007; Benedetti et al., 2008; Guerrero et  
141 al., 2011) or non-monetary units using the Operational Cost Index (Gernaey et  
142 al., 2014). However, until now no studies have incorporated energy tariff structures  
143 into the evaluation of control strategies or technologies in view of energy cost.

144 Energy demand-side mechanisms and energy tariff structures are a global trend and  
145 should be included in the evaluation of technologies and operational strategies (e.g.  
146 process control solutions). Thus, if a model-based approach has been chosen, the  
147 energy tariff structure needs to be included in the evaluation. Thus far, there still  
148 exists a gap between energy consumption and costs since there is no generalized cost  
149 model describing current energy tariff structures to evaluate operating costs at  
150 WRRFs. The energy market is very decentralized using utility-specific or client-

151 specific accounting functions to calculate energy bills. Within this context, a  
152 generalized cost model covering the major energy tariff terms enables a planning  
153 engineer to: i) Highlight critical situations where peak power demand charges are  
154 raising total energy costs; ii) Develop strategies to reduce energy consumption on a  
155 time-of-use basis and maximize energy production at peak periods; iii) Specify the  
156 appropriate equipment to reduce overall energy consumption and power demand; iv)  
157 Identify the critical terms in the energy bill and develop operating strategies to operate  
158 and control the plant for their reduction; and v) Find the optimal contracted power  
159 capacity structure for a specific plant.

160 The goal of this paper is to demonstrate the importance of incorporating more realistic  
161 energy cost models based on current energy tariff structures when evaluating  
162 operating strategies for WRRFs. For the first time within the WRRF community,  
163 generalized concepts on tariff structures are described in a systematic framework, and  
164 a generalized structure including the most common billing terms is presented. As a  
165 case study, a Spanish energy tariff structure was coupled with a WRRF process model  
166 to evaluate and compare several control strategies, thus providing insights into the  
167 selection of a specific contracted power structure. Finally, a discussion section is  
168 provided where the importance of considering energy tariff structures and future work  
169 are discussed.

170

## 171 **2. ENERGY TARIFF STRUCTURES**

172 A large variability of energy tariff structures can be found depending on: i) the  
173 customer category (i.e. residential or industrial, small or large customers); ii) the  
174 specific energy pricing structure applied; and iii) the different billing terms involved  
175 in the bill. In this section we describe the concepts of energy pricing structures and

176 billing terms behind the most common energy tariff structures for large energy  
177 customers based on selected energy contracts obtained from different WRRFs in  
178 Europe and North America.

179

## 180 **2.1. Energy pricing structures**

181 The energy pricing structure defines how the various charge rates are applied to the  
182 different terms of the bill, such as the charges related to the energy usage (expressed  
183 for example in  $\text{€}\cdot\text{kWh}^1$ ), contracting a specific power capacity (expressed as  $\text{€}\cdot\text{kV}^1$  or  
184  $\text{€}\cdot\text{kW}^1$ ) or peak power demand penalties (expressed as  $\text{€}\cdot\text{kW}^1$ ). Descriptions of the  
185 three types of energy pricing structures identified are described below.

186

### 187 *2.1.1. Flat rate structure (also called constant or fixed rate)*

188 In a flat rate structure customers are charged the same amount for the energy they use  
189 or peak power demanded, no matter the time of the day or the quantity that is  
190 consumed. This is the simplest structure but rarely applied in energy contracts for  
191 large energy customers (e.g. WRRFs).

192

### 193 *2.1.2. Time-of-Use rate structure (TOU) (also called time of day rate)*

194 TOU rate structures are widely applied at utilities across the United States and  
195 Europe. In a TOU rate, customers are charged a different price according to the time  
196 of day, day of the week and/or season of the year. **Figure 1a** shows a conceptual  
197 example of a typical TOU rate structure where different rates (P1, P2 and P3) are  
198 applied depending on the time of day. Normally, in a TOU rate two or three price  
199 periods are applied and classified as On-peak or Peak (highest energy price of the day,  
200 e.g. P1), Mid-peak or Shoulder Peak (e.g. P2), and Off-peak (lowest energy price of

201 the day, e.g. P3). The On-peak and Mid-peak periods are usually applied during the  
202 day (when the highest energy demand occurs), and the Off-peak periods during the  
203 night. The mechanism encourages customers to shift their power demand from peak  
204 periods (with high prices) to off-peak periods (with low prices). On the other hand,  
205 charge rates applied during the day can vary depending on the season or month. In the  
206 majority of the evaluated cases, a winter and summer TOU tariff schedule is defined  
207 such as in the US (e.g. Southern California Edison), where different prices and  
208 periods are applied in winter and summer, respectively. In other cases, the TOU tariff  
209 schedule can change depending on the month, such as in Spain (Royal Decree  
210 1164/2001). TOU rates are of special interest for WRRFs since usually high energy  
211 usage and power demand is linked to high load periods, usually coinciding with the  
212 highest energy price periods.

213

#### 214 *2.1.3. Tiered rate structure (also called step rate or block rate)*

215 In a tiered structure (see **Figure 1b**) customers are charged a different price based on  
216 the amount of energy used or the maximum peak power demand claimed. Various  
217 tariff blocks are defined (B1, B2 and B3), where each block is charged at a different  
218 price (P1, P2 and P3). In this way, when companies have reached the cap of their first  
219 block, any additional electricity used is charged at their second block price and so on.  
220 Depending on the type of tariff contracted, prices can increase (i.e., tiered rate) or  
221 decrease (i.e., inverse tiered rate) for the amount of energy consumed. Examples of  
222 tiered rate structures can be seen in the US (e.g. Direct Energy Business), Canada  
223 (e.g. Hydro One) and Australia (e.g. Energy Australia).

224

225

## 226 2.2. Billing terms: Understanding the electrical bill

227 The electrical bill that customers receive includes several terms, which may vary  
228 according to the specific energy tariff structure contracted. The five most common  
229 terms are summarized below.

230

231 *2.2.1 Fixed charges (also referred to as customer charges, fixed fee, fixed standing*  
232 *charges, or metering charges)*

233 The fixed charges usually cover the costs of access, metering, meter reading, billing  
234 and other customer-related operating costs. The fixed charges for each power meter  
235 [e.g. in  $\text{€}\cdot\text{month}^1$  or  $\text{€}\cdot(\text{meter}\cdot\text{month})^1$ ] are for supplying electricity to the customer  
236 premises for each day of the billing period, regardless of how much electricity is used  
237 or peak power is consumed.

238

239 *2.2.2. Fixed power charges (also referred to as power fee, contract fee, or power*  
240 *capacity charges)*

241 The fixed power or capacity charges usually cover the costs associated with the power  
242 generation and distribution. The fixed power or capacity charges are the charges to be  
243 paid depending on the defined contracted power structure, such as based on the  
244 contracted voltage [e.g.  $\text{€}\cdot(\text{kV}\cdot\text{month})^1$ ] or the contracted power capacity [e.g.  
245  $\text{€}\cdot(\text{kW}\cdot\text{month})^1$ ]. A large variability of rates and energy tariff structures (see Section  
246 2.1) can be applied depending on a number of factors (e.g. policies, regulations,  
247 electrical company, customer category, or contracted power capacity).

248

249

250 2.2.3 *Energy usage charges (also referred to as energy charges, consumption*  
251 *charges, transmission fee, or electricity supply charges)*

252 The energy usage charges usually are related to the costs sustained by the power  
253 utility for delivering electric energy to the customer, including operating and  
254 maintenance expenses of the electrical grid. The energy usage charges is varying  
255 depending to the quantity of energy consumed during the billing period (kWh), taking  
256 into account the kilowatt-hour price (e.g. €. $\text{kWh}^{-1}$ ). This term is variable depending on  
257 the amount of energy that is consumed and the energy pricing structure applied (see  
258 Section 2.1), and it often has the largest impact on the billed price.

259

260 2.2.4 *Peak power demand charges (also referred to as demand, distribution demand,*  
261 *penalty, or overuse charges)*

262 Peak power demand charges are common demand side management mechanisms used  
263 to cover the extra costs for excessive power consumption within a specified short  
264 period of time. The peak power demand charges are usually based on the maximum  
265 peak power demand (kW) measured in any time interval (e.g. 15min, 30min, or  
266 60min), in most cases during a monthly billing period or during the previous 11  
267 months, such as in the United States (e.g. Dominion Virginia Power VEPGA). There  
268 are different ways to apply peak power demand charges as shown in **Figure 2**. In the  
269 majority of cases such as in the United States (e.g. Southern California Edison) or in  
270 Sweden (e.g. Vattenfall), the peak power demand charges are determined based on the  
271 maximum peak power demand measured in a billing period (case A, **Figure 2**). In  
272 other cases, such as in Spain (Royal Decree 1164/2001), in the United States (e.g.  
273 Dominion Virginia Power VEPGA), in Sweden (e.g. E.ON Energy Company,  
274 Tekniska Verken) or Canada (e.g. Hydro Quebec), the peak power demand charges

275 are adjusted based on the difference between the maximum peak power consumed and  
276 the contracted power capacity (case B, **Figure 2**), corrected with the fixed power  
277 charges or sometimes integrated in the same billing term. If the maximum peak power  
278 consumed exceeds the contracted power, charges will be applied. For cases A and B,  
279 in order to compensate for recovering the costs of providing higher peak consumption  
280 and to discourage power demand, utilities bill the penalty charge over a monthly or  
281 quarterly cycle. This means that even though the peak power demand may only occur  
282 over a brief period of time, the customer is charged a penalty fee over a longer term.  
283 Another peak power demand charge is to apply a penalty every time the peak power  
284 demand is above the contracted power capacity (case C, **Figure 2**), such as in Spain  
285 (i.e. Royal Decree 1164/2001). Hence, the more power is consumed above the  
286 contracted power capacity, the more penalizations are applied.

287

288 *2.2.5. Reactive energy charges (also referred to as reactive power factor or reactive*  
289 *power fee)*

290 The reactive energy charges cover the costs for the energy or power dissipated by  
291 inductive electrical equipment, measured as reactive energy (kVArh) or reactive  
292 power (kVAr). The reactive energy charges are referred to the price that has to be paid  
293 when there is an excess consumption of reactive energy or power. In other words, the  
294 reactive energy charges are the charges for the inefficiency at the customer's site. The  
295 level of inefficiency is usually expressed as a percentage and is called power factor  
296 (ratio between active power and apparent power). In cases such as in Spain (Royal  
297 Decree 1164/2001), the level of inefficiency is expressed as a function of the  $\cos(\varphi)$   
298 value, where  $\varphi$  is the angle of difference (in degrees) between the active power and  
299 apparent power, which is the quantification of the departure between 1.0 (ideal

300 condition where only non-reactive power is drawn or the electrical system is fully re-  
301 phased) and the actual customer condition ( $<1.0$ ). These charges are site-specific and  
302 respond to the properties and status of the electrical equipment. A way to reduce or  
303 eliminate reactive energy charges can be by installing e.g. capacitors or replacing  
304 existing equipment (e.g. motors, transformers, or other energy consumers) with more  
305 energy-efficient equipment.

306

#### 307 2.2.6. Taxes

308 Taxes are site-specific and can include: customer taxes, energy commission taxes,  
309 regulatory taxes, delivery taxes, or green energy taxes.

310

### 311 **3. MODELLING THE TOU TARIFF STRUCTURE FROM SPAIN AND** 312 **ASSESSMENT OF CONTROL STRATEGIES**

313 This section introduces a case-study for a typical WRRF in Spain for which the  
314 Spanish energy tariff structure was modelled in detail.

315

#### 316 **3.1. Water Resource Recovery Facility under study**

317 A typical WRRF receiving a load of 115,000 population equivalents at an average  
318 flow of  $18,166 \text{ m}^3 \cdot \text{d}^{-1}$  was modelled in SIMBA# (ifak e.V., Germany) using the  
319 Benchmark Simulation Models (BSM) principles (Gernaey et al., 2014). The layout  
320 (**Figure 3**) is based on the BSM1\_LT layout, but employing the BSM2 layout reactor  
321 volumes (Gernaey et al., 2014). A tapered diffuser system was modelled with a  
322 resulting airflow split of 50% to AER1, 30% to AER2 and 20% to AER3. The  
323 original BSM blower and pump models were substituted with more detailed ones  
324 (SIMBA#, 2014). The models include variable efficiency curves, capacity bounds,

325 and parameters to mimic different types of equipment. In this case-study the model  
326 parameters were set to a constant efficiency to facilitate the results evaluation. The  
327 energy efficiency models for pumping, mixing and aeration were calibrated to achieve  
328 an energy consumption of  $0.6 \text{ kWh} \cdot (\text{PE} \cdot \text{y})^{-1}$ ,  $1.8 \text{ kWh} \cdot (\text{PE} \cdot \text{y})^{-1}$ , and  $13.7 \text{ kWh} \cdot (\text{PE} \cdot \text{y})^{-1}$   
329 respectively (Müller et al., 1999). As only the energy consumption for aeration and  
330 pumping (return activated sludge and internal recycle, wastage) was modelled, an  
331 additional constant energy consumption of  $5,543 \text{ kWh} \cdot \text{d}^{-1}$  was added to account for  
332 the extra 50% of energy (e.g. for influent pumping, heating, lighting) that a WRRF of  
333 that magnitude would consume (see **Figure 4**), which falls within the Spanish TOU-  
334 6.1 rate energy tariff structure for large energy customers (Royal Decree 1164/2001  
335 and Order ITC/2794/2007) (see Section 3.3). The dynamic BSM1\_LT influent profile  
336 of 609 days (including dynamic temperature) was simulated and the last 364 days  
337 were used for evaluation purposes (Gernaey et al., 2014).

338

### 339 **3.2. Evaluated aeration control strategies**

340 In this study three aeration control strategies based on DO and total ammonia ( $\text{NH}_x$ )  
341 measurements were implemented in SIMBA#, evaluated and compared for effluent  
342 quality, energy consumption and costs. Two different waste sludge flow rates  
343 ( $Q_{w\_winter} = 300 \text{ m}^3 \cdot \text{d}^{-1}$ ;  $Q_{w\_summer} = 400 \text{ m}^3 \cdot \text{d}^{-1}$ ) were imposed depending on the time of  
344 the year in order to sustain the nitrifying biomass in the system during the winter  
345 period. The external ( $Q_{ras} = 18,446 \text{ m}^3 \cdot \text{d}^{-1}$ ) and internal ( $Q_{intr} = 55,338 \text{ m}^3 \cdot \text{d}^{-1}$ )  
346 recirculation flow-rates remained constant throughout the simulations.

347 **Base Control Strategy:  $DO_{PI}$  control.** The DO concentration in reactor AER2 is  
348 measured and fed to a PI controller, which is manipulating the total airflow to

349 maintain a set-point of 2,5 g DO.m<sup>-3</sup>. This controller aims at achieving optimal  
350 conditions for all aerobic processes.

351 **Control Strategy 1: NH<sub>x</sub>,on-off control.** A master controller is put on top of the DO PI  
352 controller (slave). The master activates or inactivates the DO PI controller after  
353 comparing the ammonia (NH<sub>x</sub>) concentration in the last aerobic reactor (AER3) with  
354 the desired NH<sub>x</sub> set-point. The DO PI controller is switched On when the ammonium  
355 concentration is above 3.5 g NH<sub>x</sub>-N.m<sup>-3</sup> and switched Off when lower than 2.5 g NH<sub>x</sub>-  
356 N.m<sup>-3</sup>. If On, the DO PI controller uses a DO set-point of 2.5 g DO.m<sup>-3</sup>.

357 **Control strategy 2: NH<sub>x</sub>,PID control.** The total ammonia concentration in the last  
358 aerobic reactor (AER 3) is controlled at 3 g NH<sub>x</sub>-N.m<sup>-3</sup> with a master PID controller  
359 that adjusts the DO set-point for reactor AER2 between 0.1 and 2.5 g DO.m<sup>-3</sup>.

360

### 361 **3.3. TOU tariff from Spain**

362 The energy cost model was implemented in the MATLAB<sup>®</sup> platform and replicates a  
363 Spanish TOU-6.1 rate structure for large energy customers (Royal Decree 1164/2001  
364 and Order ITC/2794/2007). The TOU-6.1 rate structure is applied for a contracted  
365 voltage between 1kV and 36kV and a contracted power capacity over 450 kW. The  
366 TOU-6.1 rate structure consists of five billing terms: i) energy usage charges; ii) fixed  
367 power charges; iii) peak power demand charges; iv) reactive energy charges; and v)  
368 taxes. In this study the reactive energy charges were not included since these are site-  
369 specific (depending on the level of inefficiency of inductive electrical equipment of  
370 the customer's site) and we assume that the facility has a proper installation of these  
371 capacitors in place and there is no reactive energy. In the following sections the tariff  
372 schedule, the tariff rates and the energy cost calculations based on the different billing  
373 terms are described.

374

375 **Tariff schedule.** For the selected TOU rate structure six tariff rates (from P1 to P6)  
376 are applied during the year, but maximum three tariff rates are applied at different  
377 times of the day during a monthly billing period (see **Table 1**). On a monthly time-  
378 frame, the rates of charges applied can be classified as High (H), Moderate (M), Low  
379 (L), and Very Low (VL). The highest season charges (H) are applied during the  
380 beginning of summer (i.e. June and July) and winter seasons (i.e. December, January  
381 and February), coinciding with the highest energy demand periods of the year (e.g.  
382 increase of energy demand due to the heating/air-conditioning of households and  
383 industries). The moderate season charges (M and L) are applied during autumn and  
384 spring seasons, when the energy demand is moderate. Finally, the lowest charges  
385 (VL) are applied during holiday seasons (e.g. August), when the energy demand  
386 significantly decreases. On an hourly timeframe, the regulation of charges is  
387 performed according to the energy demand rates and the energy generation capacity  
388 during the day. The rate of charges applied can be grouped as On-peak (P1 and P3),  
389 Mid-peak (P2, P4 and P5) and Off-peak charges (P6). On-peak charges are usually  
390 applied to the highest demand periods of the day, coinciding also with the more  
391 expensive forms of electricity production (see **Table 1**). Mid-peak charges are usually  
392 applied during moderate energy demand periods. Finally Off-peak (such as night  
393 periods and weekends) charges are applied when demand is low and less expensive  
394 sources of electricity are used.

395

396 **Tariff rates.** The rates applied to the energy usage, the fixed power, and the peak  
397 power demand terms are presented in **Table 2**. These rates were obtained from a real  
398 energy contract of a WRRF and established by the electricity supplier according to the

399 Spanish legislation on average electricity tariff prices (Order IET/1491/2013). Energy  
 400 usage charges span a 2.5-fold range (from 6.58 c€.kWh<sup>-1</sup> to 16.4 c€.kWh<sup>-1</sup>), fixed  
 401 power charges span a 6-fold range [from 2.83 €.(kW.y)<sup>-1</sup> to 16.92 €.(kW.y)<sup>-1</sup>], and  
 402 peak power demand charges span a 6-fold range (from a factor of 0.17 to 1.0).

403

404 **Energy cost calculation.** The *energy usage charges* (EUC<sub>term</sub>) are calculated using  
 405 **Eq. 1** from the summation of the different energy consumption terms (EC<sub>P<sub>i</sub></sub> in  
 406 kilowatt hours - kWh) and multiplied by the corresponding charges (r<sub>VE,P<sub>i</sub></sub>) for the  
 407 different tariff periods (P<sub>i</sub>), where P<sub>n</sub> is the total number of tariff periods applied in the  
 408 electricity contract.

409

$$410 \quad \text{EUC}_{\text{term}} \left[ \frac{\text{€}}{\text{month}} \right] = \sum_{P_i=1}^{P_n} (\text{EC}_{P_i} \cdot r_{\text{VE},P_i}) \quad (\mathbf{Eq.1})$$

411

412 The *fixed power charges term* (FPC<sub>term</sub>) is the cost of selecting a specific contracted  
 413 power capacity for the different tariff periods. This is the summation of the product  
 414 between contracted power capacity (PC<sub>P<sub>i</sub></sub>, in kilowatt - kW) and charge (r<sub>FP,P<sub>i</sub></sub>), for  
 415 each tariff period. The total charges for the entire year are calculated, but then the  
 416 payment is executed proportionally every month (**Eq. 2**). If the maximum peak power  
 417 measured exceeds the contracted power capacity, then peak power demand charges  
 418 are applied (see below).

419

$$420 \quad FPC_{\text{term}} \left[ \frac{\text{€}}{\text{month}} \right] = \sum_{P_i=1}^{P_n} (PC_{P_i} \cdot r_{FP,P_i}) \cdot \left( \frac{1\text{year}}{12\text{months}} \right) \quad (\text{Eq. 2})$$

421

422 The *peak power demand charges term* ( $PDC_{\text{term}}$ ) is applied every time that the peak  
 423 power measured ( $PD_{P_i}$ , in kilowatt - kW) in a 15 minute time interval exceeds the  
 424 contracted power capacity ( $PC_{P_i}$ , in kilowatt - kW) for each tariff period (**Figure 2**,  
 425 Case C). The penalizations are accumulated and applied through the **Eq.3**, only when  
 426 the  $PD_{P_i}$  is greater than the  $PC_{P_i}$ . The total penalization is the summation of the  $n$   
 427 times of power penalized and multiplied for the specific charge factor rate ( $K_{P_i}$ ) for  
 428 each tariff period (see **Table 2**), where  $1.4064 \text{ €} \cdot \text{kW}^1$  is the corresponding charge  
 429 applied per unit of power penalized.

430

$$431 \quad PDC_{\text{term}} \left[ \frac{\text{€}}{\text{month}} \right] = \sum_{P_i=1}^{P_n} ( 1.4064 \cdot K_{P_i} \cdot \sqrt{\sum_{j=1}^{j=n} (PC_{P_i} - PD_{P_i})^2} ) \quad (\text{Eq. 3})$$

432

433 A *taxation term* ( $T_{\text{term}}$ ) is applied to the sum of the variable energy, the fixed power,  
 434 and the penalty term. In Spain, the tax on electricity is 4.28% and the national value-  
 435 added tax (VAT) is 21% applied on the taxed gross. Hence, the *total energy cost*  
 436 (TEC) is the resulting sum of the different charge terms, as defined in **Eq. 4**:

437

$$438 \quad TEC \left[ \frac{\text{€}}{\text{month}} \right] = EUC_{\text{term}} + FPC_{\text{term}} + PDC_{\text{term}} + T_{\text{term}} \quad (\text{Eq. 4})$$

439

## 440 4. RESULTS

### 441 4.1. Information provided by the new energy cost model

442 In this section an illustrative example of the implemented energy cost model for the  
 443 one year simulation period of the Base Control Strategy (DO PI controller,  $DO_{PI}$ ) is

444 presented. In this study, 500 kW of contracted power capacity is selected for all tariff  
445 periods (P1 to P6).

446

#### 447 *4.1.1 Billing terms contribution for each month*

448 **Figure 5** shows monthly costs (split amongst the different billing terms) over the one  
449 year simulation of the DO<sub>PI</sub> strategy. The results of the energy cost model show a  
450 large variability in costs (from 30,068 to 52,748 €month<sup>-1</sup>) (see stacked bar in **Figure**  
451 **5**). The billing terms contributing most to the overall energy costs are the energy  
452 usage charges (accounting for 69% to 74% of the monthly total energy costs),  
453 followed by the total taxes (~ 21%), the fixed power charges (4 to 7%) and finally the  
454 peak power demand charges (0 to 5%). With regards to the variability of these terms,  
455 the fixed power is the only term that remains constant throughout the year, while the  
456 energy usage, the peak power demand charges and taxes are particularly variable.

457

#### 458 *4.1.2 Comparing the real energy cost model with an average energy price*

459 The real cost model is compared with the case of using an average energy price (see  
460 line in **Figure 5**) of 12 c€/kWh<sup>1</sup>, calculated based on the total costs and the total  
461 energy consumed for one year simulation of the selected Base Control Strategy. The  
462 costs obtained when using an average energy price are only depending on the energy  
463 consumption and therefore show less variability over the months (from 37782 to  
464 42411 €.month<sup>1</sup>). A control scenario evaluation using a simplified cost model based  
465 on an average energy price would therefore result in cost differences of 7 to 30%  
466 when compared to the real energy cost model, with significant over-estimation (30%  
467 in August, coinciding with the lowest rates) and under-estimation (22% in July,  
468 coinciding with the highest rates). The main reason for the differences between real

469 cost models and average energy prices stems from the rates applied to the energy  
470 usage and peak power demand charges (see **Table 1** and **Table 2**), which are much  
471 higher during On-peak periods when compared to Off-peak periods. The rates for the  
472 peak power demand charges are 6 times higher during Off-peak periods, but with less  
473 contribution (1-5%) compared to the energy usage charges (69-73%). The “average  
474 energy price” used in the comparison is calculated from the total energy cost and the  
475 total energy consumed for the Base Control Strategy over the whole evaluation period  
476 (1 year), and therefore the annual difference between the proposed energy cost model  
477 and the average energy price is zero.

478

#### 479 *4.1.3 On-peak, Mid-peak and Off-peak contributions to the energy usage charges*

480 **Figure 6** shows the monthly total energy consumed distributed by tariff periods  
481 (**Figure 6a**) and the related energy usage charges (**Figure 6b**). The total energy  
482 consumed (**Figure 6a**) remains close to  $363 \text{ MWh}\cdot\text{month}^{-1}$  (coefficient of variation of  
483 0.03) with around 16% during the On-peak periods, 24% during the Mid-peak  
484 periods, and 55% during the Off-peak periods. With regards to the energy usage  
485 charges (**Figure 6b**), larger variability compared to the total energy consumption was  
486 observed (21,518 to  $37,294 \text{ €}\cdot\text{month}^{-1}$ ) corresponding to a coefficient of variation of  
487 0.17.

488

#### 489 *4.1.4 On-peak, Mid-peak and Off-peak contributions on the peak power demand* 490 *charges*

491 **Figure 7** shows the total power penalized distributed by tariff periods (**Figure 7a**) and  
492 the related peak power demand charges (**Figure 7b**). The total power penalized  
493 (**Figure 7a**) is highly variable during the year ranging from 2.7 to  $3,045 \text{ kW}\cdot\text{month}^{-1}$ .

494 With regards to the distribution of the power penalties through the different tariff  
495 periods, between 36-49% is assigned to On-peak periods, 36-43% to Mid-peak  
496 periods, and around 19% to Off-peak periods. Regarding the related costs, peak power  
497 demand charges (**Figure 7b**) are highly variable during the year (from 32 to 2,342  
498 €·month<sup>1</sup>). It is worth noting that during the winter period the penalizations are very  
499 low which is related to the response of the DO PI control under low temperatures  
500 which is smoother.

501

## 502 **4.2. Evaluation of aeration control strategies using the new cost model**

503 In this section the results for the two ammonia-based aeration control strategies are  
504 compared against the Base Control Strategy and evaluated for the one year simulation  
505 period and maintaining the selected contracted power capacity of 500 kW for all the  
506 strategies.

507

### 508 *4.2.1 Evaluation of system performance*

509 **Figure 8** shows the yearly average results obtained in terms of system performance  
510 and costs for the DO<sub>PI</sub>, NH<sub>x,ON/OFF</sub> and NH<sub>x,PID</sub> controllers. The yearly average total  
511 NH<sub>x</sub> concentration for the DO<sub>PI</sub> controller (targeting full nitrification) is  
512 approximately 1.0 g NH<sub>x</sub>-N·m<sup>-3</sup>. Full nitrification could not be reached due to the high  
513 variability of the influent NH<sub>x</sub> load compared to the slow changing mass of active  
514 nitrifiers (Rieger et al., 2014). The total nitrogen concentration is approximately 12.8  
515 g NH<sub>x</sub>-N·m<sup>-3</sup> (**Figure 8a**). By introducing an NH<sub>x</sub> controller the yearly average NH<sub>x</sub>  
516 concentration increases (the total ammonia set-point for the NH<sub>x,PID</sub> is set to 3.0 g  
517 NH<sub>x</sub>-N·m<sup>-3</sup> and the switching criteria for the NH<sub>x,ON/OFF</sub> controller are set to 2.5 - 3.5 g  
518 NH<sub>x</sub>-N·m<sup>-3</sup>). At the same time total nitrogen (TN) decreases by 25%, reaching 9.5g

519  $\text{N}\cdot\text{m}^{-3}$ . The  $\text{NH}_{\text{x,ON/OFF}}$  and  $\text{NH}_{\text{x,PID}}$  controllers reduce aeration energy consumption by  
520 7% and 18%, respectively, when compared to the  $\text{DO}_{\text{PI}}$ . When considering the total  
521 energy consumption in the WRRF, the savings translate to 3 and 7%, respectively,  
522 when compared to the  $\text{DO}_{\text{PI}}$ . Overall, the  $\text{NH}_{\text{x,PID}}$  controller shows the best results in  
523 terms of nitrogen removal and energy consumption, followed by the  $\text{NH}_{\text{x,ON/OFF}}$  and  
524 the  $\text{DO}_{\text{PI}}$  controllers.

525

#### 526 4.2.2. Evaluation of the energy costs

527 **Figure 8b** shows the energy costs for one year obtained after simulating the three  
528 aeration control strategies using the new energy cost model (coloured bars) and  
529 compared with the case of using an average energy price (shadowed bars). The results  
530 indicate that the best control strategy is still the  $\text{NH}_{\text{x,PID}}$  ( $461,717 \text{ €y}^{-1}$ ), resulting in  
531 9% and 5% lower costs when compared to the  $\text{DO}_{\text{PI}}$  ( $485,014 \text{ €y}^{-1}$ ) and the  
532  $\text{NH}_{\text{x,ON/OFF}}$  ( $508,693 \text{ €y}^{-1}$ ), respectively. With the new and more realistic energy cost  
533 model, the total energy costs for the  $\text{NH}_{\text{x,ON/OFF}}$  controller are even higher than the  
534 Base Control Strategy due to the high impact of the penalization term (see **Figure**  
535 **8b**). PID or PI control strategies have a more attenuated response to disturbances than  
536 the digital On/Off control strategy, thus avoiding a sharp switch in DO set-points and  
537 consequently a sudden acceleration or turn-down of the blowers. Hence, the selection  
538 of best operating strategies (or in this case control strategies) cannot only rely on  
539 energy consumption, but should include variable energy pricing structures and the  
540 different billing terms.

541

542

543

### 544 4.3. Scenario analysis for selecting the optimal contracted power capacity

545 The energy market is highly dynamic and we observe a tendency to increase rates,  
546 especially for the fixed power and peak power demand terms. For instance,  
547 Albadalejo and Trapote (2013) studied the effects of electricity tariffs on the operating  
548 costs of WRRFs in Spain, concluding that the revision of the electricity rates between  
549 2009 and 2012 have resulted in increases of electricity costs of 64.5% and 79% for  
550 small and large WRRFs, respectively. This caused an increase of electricity costs of  
551 the overall operating costs from 44% to 56%. As a consequence, this has motivated  
552 WRRFs to revise their electricity contracts by adjusting the contracted power capacity  
553 (hence, decreasing the charges for the fixed or the penalty charges in the bill).  
554 However, when lowering the contracted power the risk of getting penalization  
555 increases. Such a trade-off can only be properly assessed using a realistic energy cost  
556 model as shown in **Figure 9**.

557 For the case-study presented before different contracted power values (from 500 kW  
558 to 800kW) were evaluated for the tested control strategies. **Figure 9** shows the results  
559 in terms of total energy costs (**Figure 9a**), the peak power demand charges (**Figure**  
560 **9b**) and the cost differences with an average energy price (**Figure 9c**). The results  
561 show that total costs (**Figure 9a**) can be reduced by finding the optimal contracted  
562 power which is 550 kW for the  $DO_{PI}$ , 600 kW for the  $NH_{x,PID}$  and 750 kW for the  
563  $NH_{x,ON/OFF}$  controllers. Peak power demand charges can significantly be reduced by  
564 increasing the contracted power capacity (**Figure 9b**), although at the expense of a  
565 slight increase in fixed costs. Hence, savings of  $5,335 \text{ €y}^{-1}$  or 1% can be achieved for  
566 the  $DO_{PI}$ ,  $26,333 \text{ €y}^{-1}$  or 5% for the  $NH_{x,ON/OFF}$ , and  $8,124 \text{ €y}^{-1}$  or 2% for the  $NH_{x,PID}$   
567 controllers, when comparing to the default contracted power of 500kW. After  
568 considering the increase in the contracted power capacity the aeration control strategy

569 resulting in the lowest costs is still the  $NH_{x,PID}$  strategy with savings of ~6% when  
570 compared to the  $DO_{PI}$  and the  $NH_{x,ON/OFF}$  controllers.

571 Finally, **Figure 9c** shows the percent difference between the energy cost resulting  
572 from the constant energy price and the proposed realistic energy cost model. The  
573 results show that the percentage is not constant depending on the contracted power  
574 and the aeration strategy. Using a simplified cost model based on averages would  
575 result in an average monthly cost difference of 13-15% when compared to the realistic  
576 energy cost model. A monthly cost deviation of 6-10% was calculated depending on  
577 the specific month, the control strategy and the contracted power selected. A  
578 maximum difference of 25% was reached for the  $NH_{x,ON/OFF}$  at 500 kW contracted  
579 power.

580

## 581 **5. DISCUSSION**

### 582 **5.1 Importance of considering energy tariff structures**

583 This paper presents a framework to model energy tariff structures and a case study  
584 demonstrating the importance of taking energy tariff structures into account when  
585 comparing control strategies or technologies in WRFs. In most energy studies the  
586 energy cost is produced by multiplying the energy consumption by an average energy  
587 price. However, we demonstrate here that operating costs depend significantly on the  
588 energy tariff structure applied, where different energy pricing structures (e.g., TOU)  
589 and/or peak demand penalty charges may alter substantially the cost efficiency of a  
590 control strategy. Therefore, reducing energy consumption does not necessarily mean  
591 reducing energy costs, and hence proper cost models are required to select the best  
592 control strategy.

593 The implementation of energy tariff structures offers the opportunity to better  
594 understand the energy costs of WWRFs, thereby being able to build an operational  
595 strategy through which the minimization of energy costs is obtained while  
596 maintaining the required effluent quality. First, the main energy cost contributors  
597 should be identified by analysing: i) the energy dynamics; ii) the impact of the energy  
598 tariff structure applied; iii) the way the different terms are calculated; iv) the role of  
599 the power terms and their contributions; and finally v) the potentials for further  
600 energy cost minimization. Then, several measures could be applied, including: i)  
601 avoiding peak power demand, especially during On-Peak periods; ii) shifting energy  
602 consumption from On-peak to Off-peak periods; and/or iii) coordinating in-plant  
603 power generation to reduce peak demands. The first option implies setting proper  
604 maximum boundaries for the controller settings together with proper selection of the  
605 contracted power capacity. The second option ranges from inexpensive measures  
606 (e.g., changing controller set-points and parameters for the different periods) to more  
607 expensive measures such as the construction of equalization basins, where possible.  
608 The third option could be coordinated on a plant level or even on an electrical grid  
609 level by shifting the control of biogas-fuelled generators to the energy provider. The  
610 plant should then benefit from a reduced energy tariff.

611

## 612 **5.2 Outlook**

613 The consideration of energy tariff structures in the management of WWRFs is the  
614 next natural step especially for WWRFs. Hence, depending on the effluent limits  
615 established, while maintaining the effluent limits below the never-to-exceed limits, a  
616 wide range of operational strategies could be applied (see previous section). On the  
617 other hand, a wide range of energy tariff structures can be found with different energy

618 pricing structures (e.g., TOU, Tiered) and different ways to apply peak power demand  
619 charges. Within this context, further work is needed in the evaluation of the benefits  
620 and effects on energy costs of combinations of the above listed options.

621 Finally, the interdependency of water and energy systems is undeniable and opens the  
622 opportunity for better management of both. This is of special importance with  
623 WWRFs where the highest energy consumption usually coincides with the highest  
624 peak demand load on the power grid, thus coinciding with the highest energy price  
625 periods. Hence, reducing peak power demand in a short periods when energy cost are  
626 highest will also benefit the energy system by reducing grid load and GHG emissions  
627 (due to the need for more carbon-intensive energy sources during peak power demand  
628 periods). The impact of reducing peak demand in urban wastewater systems and the  
629 resulting benefits in the energy system in terms of energy generation costs and GHG  
630 emissions should be studied. These studies would be even more pertinent to regions  
631 experiencing extended droughts, since the ability to generate power depends on that  
632 of water, and water-stress conditions may imply limits on the ability for power  
633 utilities to deliver peak demand.

634

## 635 **6. CONCLUSIONS**

636 This paper demonstrates the importance of incorporating realistic cost models for the  
637 operational optimization of WRRFs. A new energy cost model based on actual energy  
638 tariffs was introduced and as a case study a Spanish tariff was successfully tested on a  
639 benchmark platform to evaluate different control strategies. It was demonstrated that  
640 the use of an average price for energy cost evaluation of WRRF operating strategies  
641 does not provide realistic costs. For the case study evaluated, monthly cost differences  
642 of 7 to 30% were observed compared to the proposed realistic energy cost model for a

643 WRRF operating with a DO PI control strategy. In the evaluation and aeration control  
644 strategies, it was demonstrated that using average energy prices and neglecting energy  
645 tariff structures may lead to biased conclusions when selecting operating strategies  
646 (e.g. control solutions) or comparing technologies or equipment. The results also  
647 demonstrated that selecting the optimal power contracted is a key issue since different  
648 operating strategies result in different optimal contracted power, and hence, proper  
649 energy cost models are required.

650 Energy cost calculations are very site-specific and it is therefore important to take into  
651 account the local energy tariff when evaluating operational strategies or selecting  
652 technologies or equipment. The proposed generic energy tariff model structure has  
653 been derived from various tariffs from around the world and can be used to implement  
654 individual energy tariffs.

655

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664

665

666 **8. REFERENCES**

- 667 Albadalejo A. & Trapote A. (2013). The effect of electricity tariffs on the operating  
668 costs of the wastewater treatment plants (Influencia de las tarifas eléctricas en los  
669 costes de operación y mantenimiento de las depuradoras de aguas residuales).  
670 *Tecnoaqua*, Sep-Oct 2013 (3), 48-54.  
671 [http://issuu.com/infoedita/docs/tecnoaqua\\_sep-](http://issuu.com/infoedita/docs/tecnoaqua_sep-)  
672 [octubre\\_2013/51?e=8341277/5549729](http://issuu.com/infoedita/docs/tecnoaqua_sep-octubre_2013/51?e=8341277/5549729) (accessed 11.12.2014) [in Spanish].  
673
- 674 Amand, L., Olsson, G. & Carlsson, B. (2013). Aeration Control - A Review. *Water*  
675 *Sci. Technol.*, 67 (11), 2374–2398.  
676
- 677 Benedetti, L., Dirckx, G., Bixio, D., Thoeye, C. & Vanrolleghem, P.A. (2008).  
678 Environmental and economic performance assessment of the integrated urban  
679 wastewater system. *Journal of Environmental Management*, 88 (4), 1262-1272.  
680
- 681 Cadet, C., Beteau, J.F. & Hernandez, S.C. (2004). Multicriteria control strategy for  
682 cost/quality compromise in wastewater treatment plants. *Control Engineering*  
683 *Practice*, 12 (3), 335-347.  
684
- 685 Ekman, M., Björleinius, B. & Andersson, M. (2006). Control of the aeration volume in  
686 an activated sludge process using supervisory control strategies. *Water Res.*, 40  
687 (8), 1668-1676.  
688

- 689 Gernaey, K.V., Jeppsson, U., Vanrolleghem, P.A., Copp, J.B. (2014), Benchmarking  
690 of Control Strategies for Wastewater Treatment Plants. IWA Scientific and  
691 Technical Report No. 23, ISBN 9781843391463, IWA Publishing, London, UK.  
692
- 693 Guerrero, J., Guisasola, A., Vilanova, R. & Baeza, J.A. (2011). Improving the  
694 performance of a WWTP control system by model-based setpoint optimisation.  
695 Environmental Modelling & Software, 26(4), 492-497.  
696
- 697 Leu, S.Y. Rosso, D., Larson, L.E. & Stenstrom, M.K. (2009). Real-time aeration  
698 efficiency monitoring in the activated sludge process and methods to reduce  
699 energy consumption and operating costs. Water Environ. Res., 81 (12), 2471-  
700 2481.  
701
- 702 Müller, E.A., Kobel, B., Künti, T., Pinnekamp, J., Seibert-Erling, G., Schaab, R. &  
703 Böcker, K. (1999). Manual energy in wastewater plants (Handbuch Energie in  
704 Kläranlagen). Ministry of Environment, Physical Planning and Agriculture of  
705 North Rhine-Westphalia, Germany [in German].  
706
- 707 Olsson, G. (2012b). ICA and me - A subjective review. Water Res., 46 (6), 1585-  
708 1624.  
709
- 710 Olsson, G. (2012a). Water and energy: threats and opportunities. IWA Publishing,  
711 London, UK.  
712

- 713 Order IET/1491/2013. Revising the access tariffs of electricity for its implementation  
714 from August 2013 and for which certain tariffs and bonus for special regime  
715 facilities for the second quarter of 2013 are reviewed (Orden IET/1492/2013 por  
716 la que se revisan los peajes de acceso de energía eléctrica para su aplicación a  
717 partir de agosto de 2013 y por la que se revisan determinadas tarifas y primas de  
718 las instalaciones del régimen especial para el segundo trimestre de 2013).  
719 Available at <https://www.boe.es/boe/dias/2013/08/03/pdfs/BOE-A-2013-8561.pdf>  
720 [in Spanish].  
721
- 722 Order ITC/2794/2007. Revising the electricity tariffs from October 1, 2007 (Orden  
723 ITC/2794/2007, de 27 septiembre, por la que se revisan las tarifas eléctricas a  
724 partir del 1 de octubre de 2007). Available at  
725 <https://www.boe.es/boe/dias/2007/09/29/pdfs/A39690-39698.pdf> [in Spanish].  
726
- 727 Palensky, P. & Dietrich, D. (2011). Demand side management: Demand response,  
728 intelligent energy systems, and smart loads. *Industrial Informatics, IEEE*  
729 *Transactions on*, 7 (3), 381-388.  
730
- 731 Royal Decree 1164/2001. Establishing the charges for access to the transmission and  
732 distribution of electricity access (Real Decreto 1164/2001, de 26 de octubre, por el  
733 que se establecen tarifas de acceso a las redes de transporte y distribución de  
734 energía eléctrica). Available at  
735 <https://www.boe.es/boe/dias/2001/11/08/pdfs/A40618-40629.pdf> [in Spanish].  
736
- 737 Reardon, D.J. (1995). Turning down the power. *Civ. Eng.*, 65 (8), 54-56.

738

739 Rieger, L., Jones, R.M., Dold, P.L. & Bott, C.B. (2014). Ammonia-based feedforward  
740 and feedback aeration control in activated sludge processes. *Water Environ. Res.*,  
741 86 (1), 63-73.

742

743 Rosso, D. & Stenstrom, M.K. (2005). Comparative economic analysis of the impacts  
744 of mean cell retention time and denitrification on aeration systems. *Water Res.*, 39  
745 (16), 3773-3780.

746

747 Samuelsson, P., Halvarsson, B. & Carlsson, B. (2007). Cost-efficient operation of a  
748 denitrifying activated sludge process. *Water Res.*, 41 (11), 2325-2332.

749

750 Spees, K. & Lave, L. (2008). Impacts of responsive load. In *PJM: Load shifting and*  
751 *real time pricing*. *The Energy Journal*, 101-121.

752

753 SIMBA# (2014). SIMBA# version 1.1.36: Advanced Manual. ifak e. V., Magdeburg,  
754 Germany.

755

756 Stare, A., Vrečko, D., Hvala, N. & Strmčnik, S. (2007). Comparison of control  
757 strategies for nitrogen removal in an activated sludge process in terms of operating  
758 costs: a simulation study. *Water Res.*, 41 (9), 2004-2014.

759

760 Water Environment Federation - WEF (2009). *Energy conservation in water and*  
761 *wastewater facilities (MOP 32)*. WEF Publishing, Alexandria, VA, USA.

762

763 **TABLES**

764 **Table 1** - Tariff periods distribution during week days applied in a TOU-6.1 energy  
765 tariff structure (powers contracted up to 500kW) from the peninsula's Spanish  
766 Electricity System. During weekends (from 0 to 24h) only the P6 tariff period is  
767 applied. Months are classified based on the charges depending of the tariff rates  
768 applied (VL = Very Low, L = Low, M = Medium, and H = High).

769

770 **Table 2** - Unit charges applied for a TOU-6.1 energy tariff structure for a real WRRF  
771 - High Voltage power contract of 500 kW

772

773 **LIST OF FIGURES**

774

775 **Figure 1.** Example of different energy pricing structures: a) Time-of-Use rate with 3  
776 tariff periods: On-peak (P1), Mid-peak (P2) and Off-peak (P3), and b) Tiered rate  
777 with 3 blocks (B1, B2 and B3) and charges rate (P1, P2 and P3). The grey line (left  
778 axis) represents the energy consumption or the power demand rate in Figure 1a, and  
779 the total energy consumed or maximum peak power demanded in Figure 1b. The  
780 black line (dark) represents the charges rate applied.

781

782 **Figure 2.** Types of power demand charges that can be applied: Case A, Case B, and  
783 Case C. The grey line (left axis) represents the power demand rate and the dark line  
784 the contracted power capacity.

785

786 **Figure 3.** Layout of the WRRF plant under study. Two levels of control are shown:  
787 DO control and  $\text{NH}_x$  which manipulates the DO set-point.

788

789 **Figure 4.** Average electricity consumption with the corresponding distribution of  
790 energy consumptions from the different process units of the modelled WRRF.

791

792 **Figure 5.** Energy cost evaluation by using a) the proposed energy cost model (bar  
793 plot) and b) average energy price (line plot). The energy costs obtained from the  
794 energy cost model are disaggregated in the terms involved in the selected TOU energy  
795 tariff structure (i.e. fixed power charges, energy usage charges, power demand  
796 charges, and taxes).

797

798 **Figure 6.** Evaluation of the  $DO_{PI}$  control strategy in terms of a) total energy  
799 consumed and the corresponding b) energy usage charges per month taking time-of-  
800 use periods into account.

801

802 **Figure 7.** Evaluation of the  $DO_{PI}$  control strategy in terms of a) total power penalized  
803 and the corresponding b) peak power demand charges per month taking time-of-use  
804 periods into account.

805

806 **Figure 8.** Yearly evaluation of the simulated control strategies: a) TN effluent  
807 concentrations and total energy consumed, and b) Energy cost model versus average  
808 energy price.

809

810 **Figure 9.** Impact of the power contracted on the total power term for the different  
811 strategies evaluated. No bar in Fig 8b means  $0 \text{ €}\cdot\text{year}^{-1}$ . Stacked bars in Fig 8c  
812 correspond to the average of the monthly absolute differences, and the error bars  
813 correspond to the standard deviation for the 12 months evaluated.

1 **Table 1** - Tariff periods distribution during week days applied in a TOU-6.1 energy  
 2 tariff structure (powers contracted up to 500kW) from the peninsula's Spanish  
 3 Electricity System. During weekends (from 0 to 24h) only the P6 tariff period is  
 4 applied. Months are classified based on the charges depending of the tariff rates  
 5 applied (VL = Very Low, L = Low, M = Medium, and H = High).

	Hours of the day (h)																								Season
	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	
January	P6				P2		P1			P2				P1			P2				H				
February	P6				P2		P1			P2				P1			P2				H				
March	P6				P4								P3				P4				M				
April	P6				P5																				L
May	P6				P5																				L
1-15 <sup>th</sup> June	P6				P4	P3				P4											M				
16-30 <sup>th</sup> June	P6				P2		P1						P2						H						
July	P6				P2		P1						P2						H						
August	P6																								VL
September	P6				P4	P3				P4											M				
October	P6				P5																				L
November	P6				P4								P3				P4				M				
December	P6				P2		P1			P2				P1			P2				H				

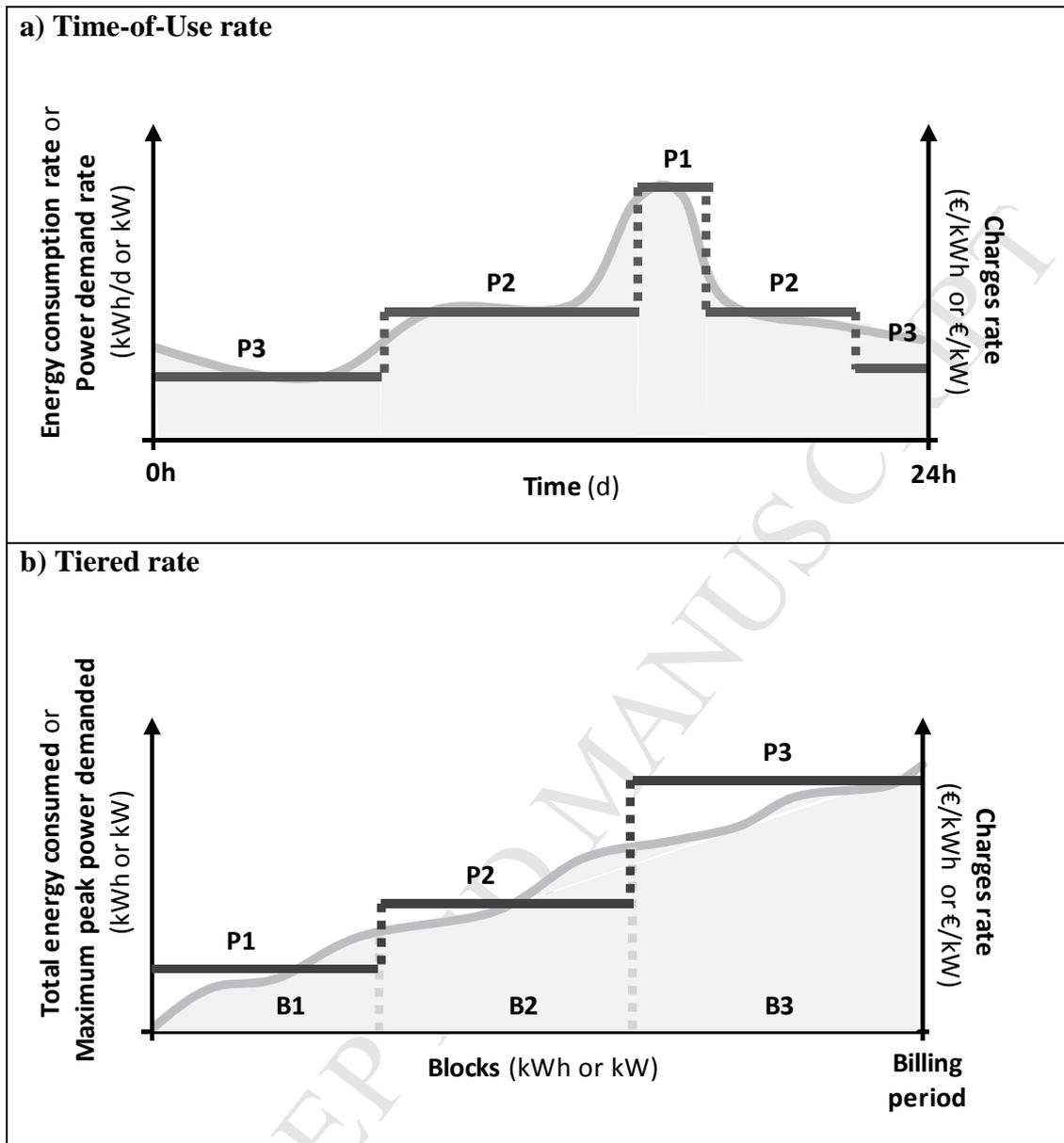
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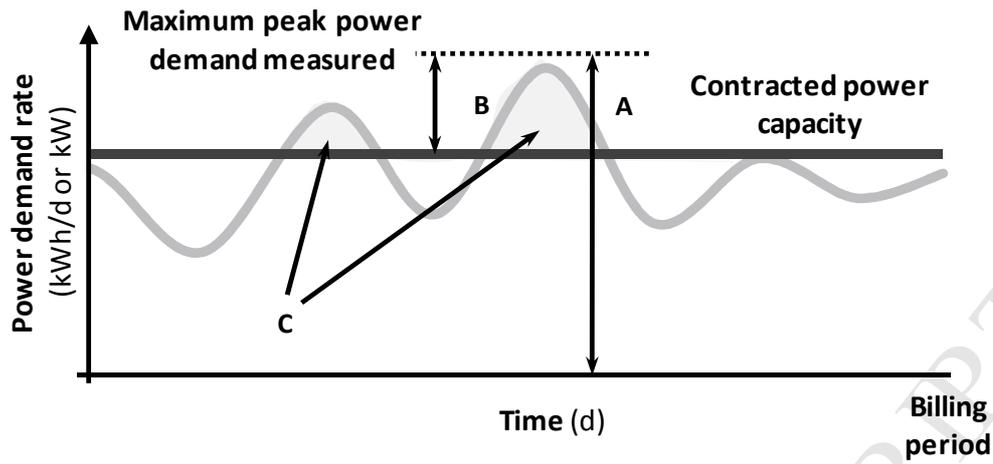
**Table 2** - Unit charges applied for a TOU-6.1 energy tariff structure for a real WRRF  
- High Voltage power contract of 500 kW

Unit charges	P1	P2	P3	P4	P5	P6	Units
Energy usage rates ( $r_{VE,P_i}$ )	16.4	13.2	11.0	8.6	8.0	6.58	c€.kWh <sup>1</sup>
Fixed power rates ( $r_{FP,P_i}$ )	16.92	8.47	6.20	6.20	6.20	2.83	€.(kW.year) <sup>1</sup>
Peak power demand rates ( $K_{P_i}$ )	1	0.5	0.37	0.37	0.37	0.17	-

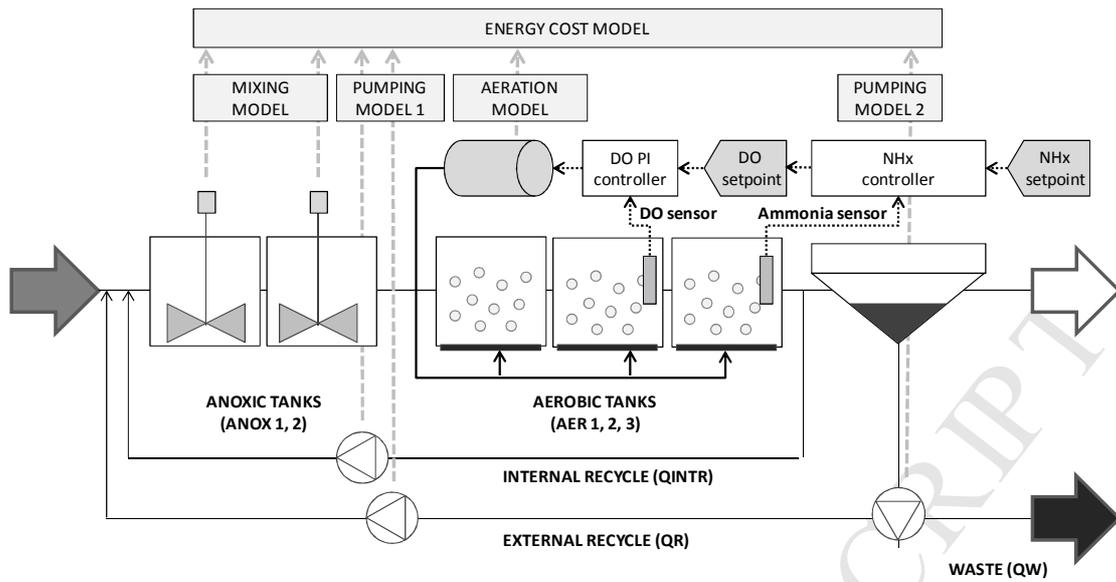
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**Figure 1.** Example of different energy pricing structures: a) Time-of-Use rate with 3 tariff periods: On-peak (P1), Mid-peak (P2) and Off-peak (P3), and b) Tiered rate with 3 blocks (B1, B2 and B3) and charges rate (P1, P2 and P3). The grey line (left axis) represents the energy consumption or the power demand rate in Figure 1a, and the total energy consumed or maximum peak power demanded in Figure 1b. The black line (dark) represents the charges rate applied.

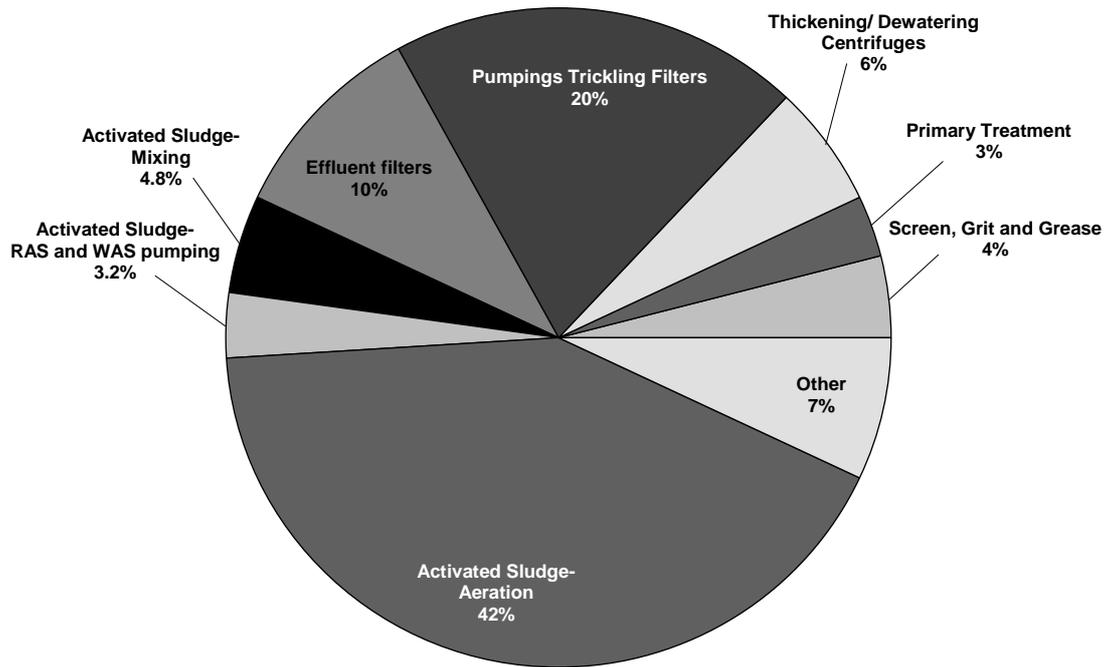


**Figure 2.** Types of power demand charges that can be applied: Case A, Case B, and Case C. The grey line (left axis) represents the power demand rate and the dark line the contracted power capacity.

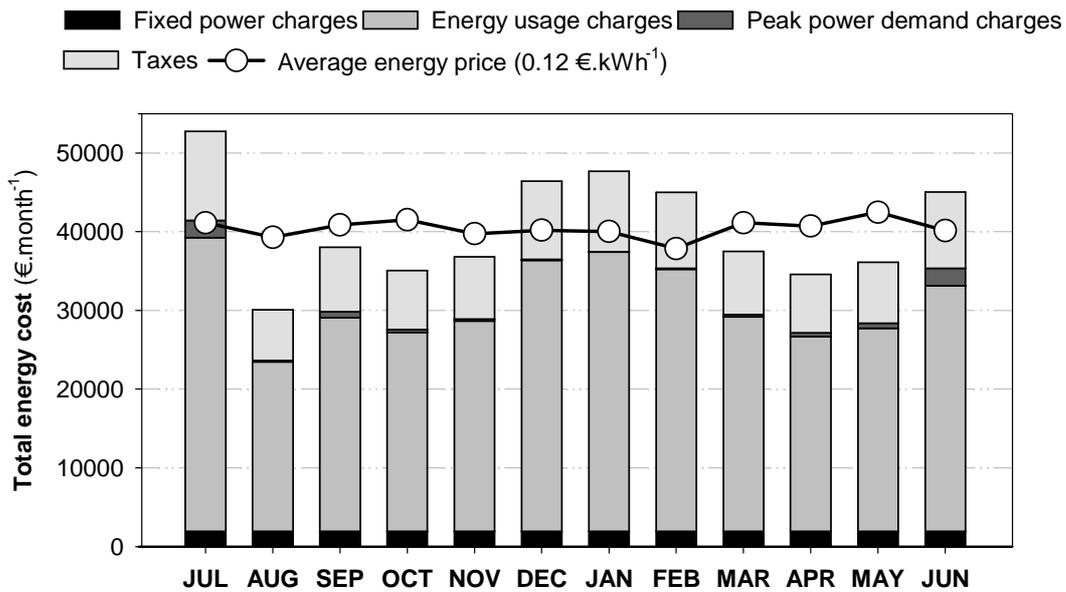


**Figure 3.** Layout of the WRRF plant under study. Two levels of control are shown: DO control and NH<sub>x</sub> which manipulates the DO set-point.

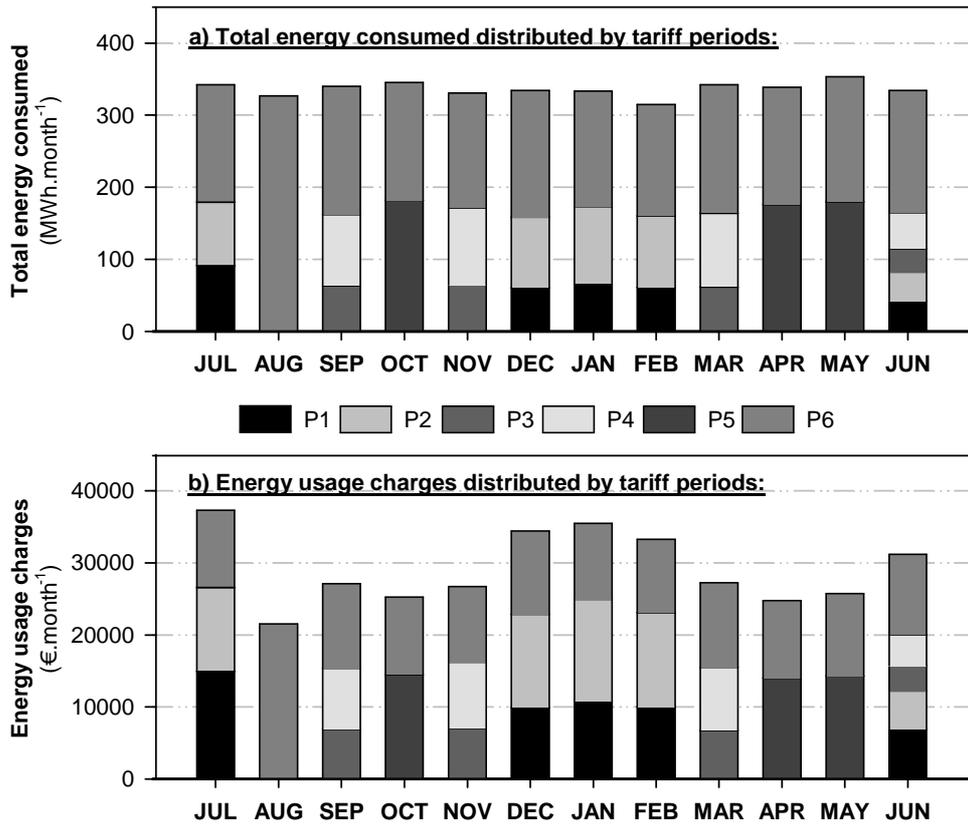
## Average Electricity Consumption of the modeled WRRF



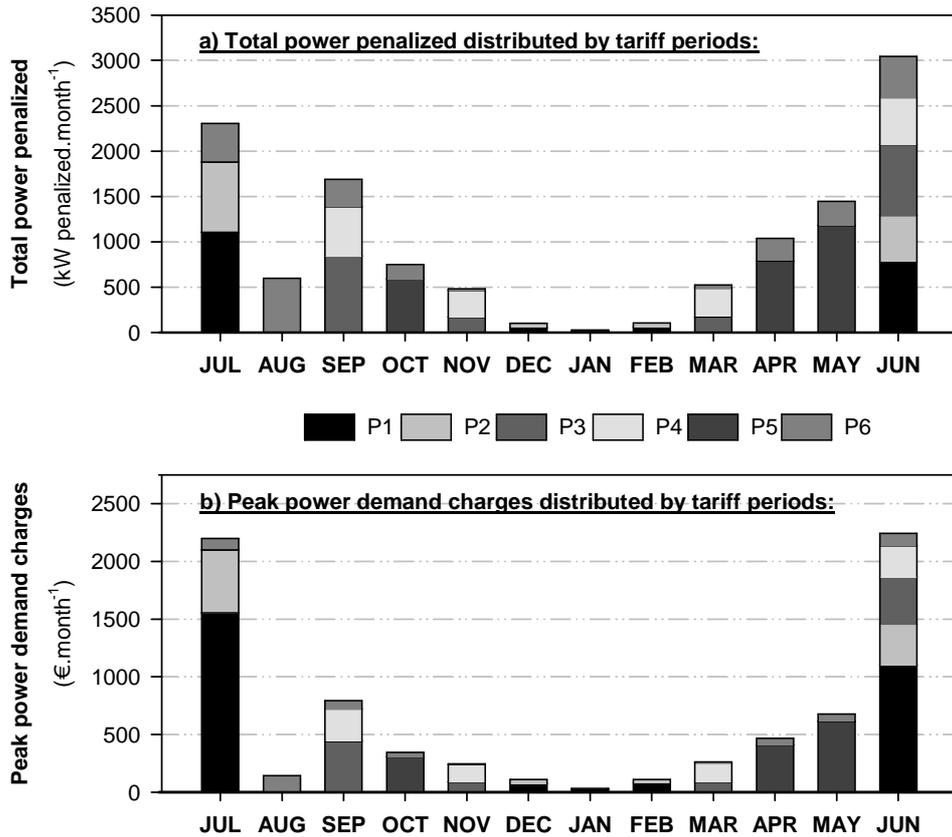
**Figure 4.** Average electricity consumption with the corresponding distribution of energy consumptions from the different process units of the modelled WRRF.



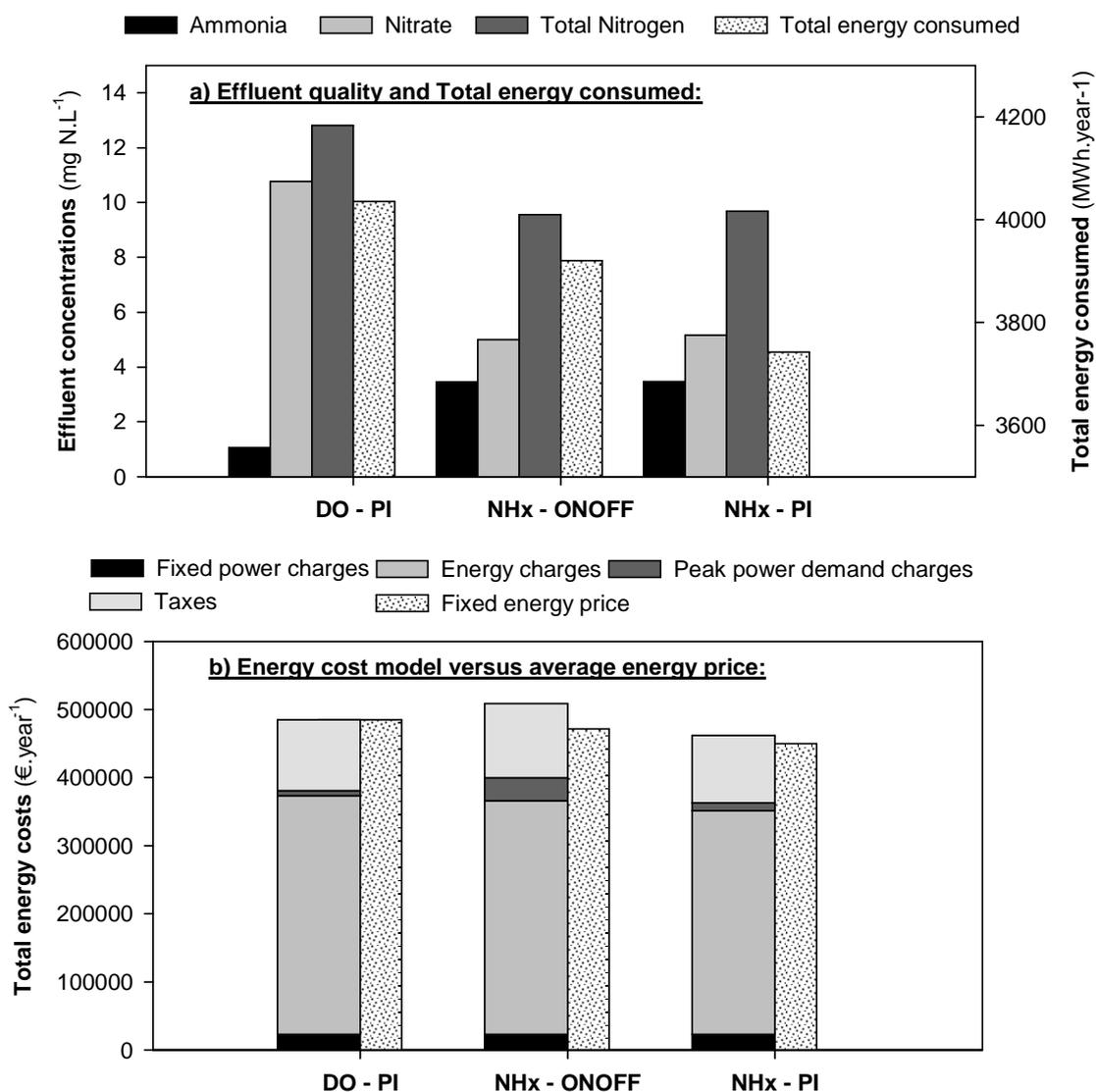
**Figure 5.** Energy cost evaluation by using a) the proposed energy cost model (bar plot) and b) average energy price (line plot). The energy costs obtained from the energy cost model are disaggregated in the terms involved in the selected TOU energy tariff structure (i.e. fixed power charges, energy usage charges, power demand charges, and taxes).



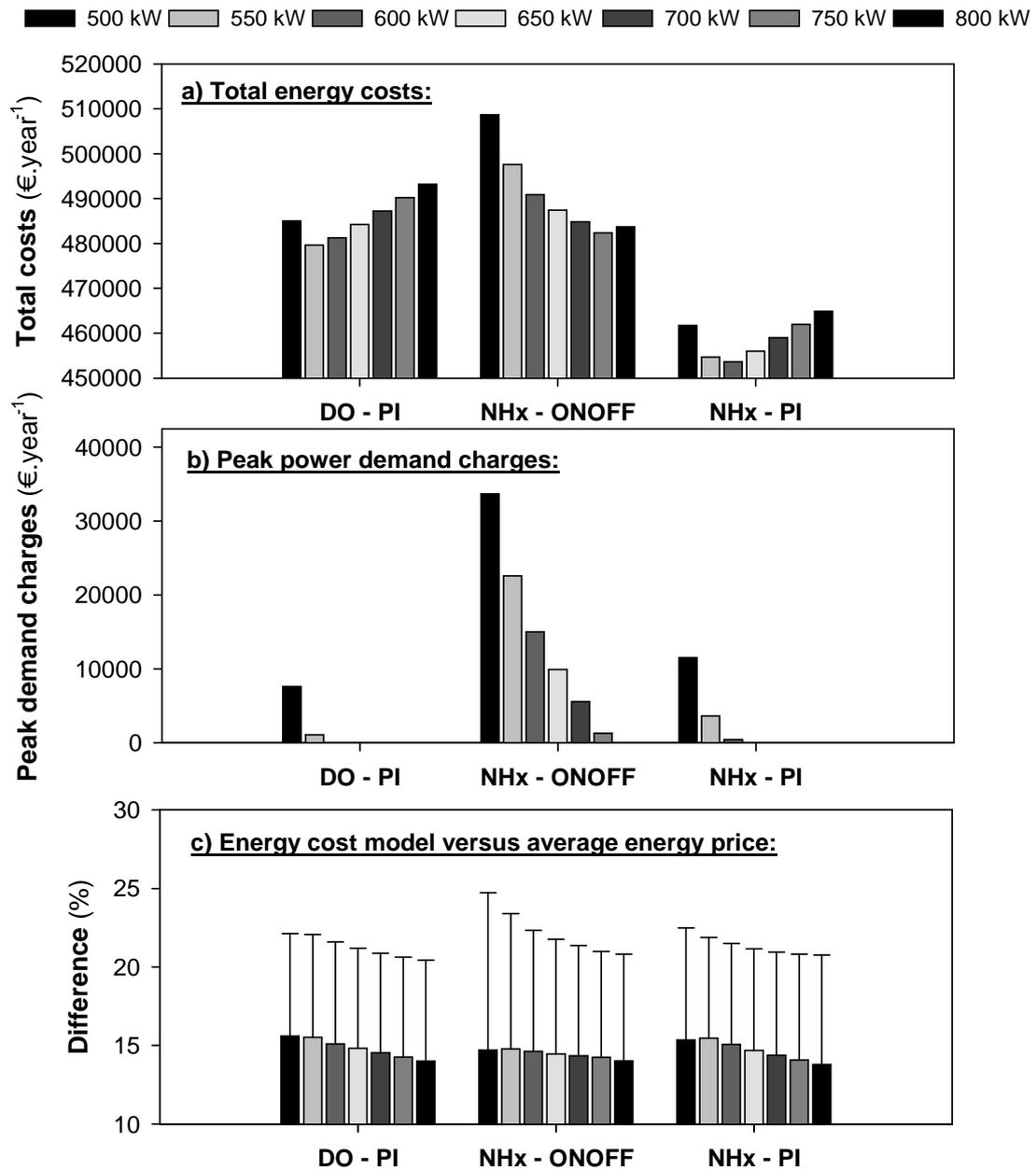
**Figure 6.** Evaluation of the  $DO_{PI}$  control strategy in terms of a) total energy consumed and the corresponding b) energy usage charges per month taking time-of-use periods into account.



**Figure 7.** Evaluation of the  $DO_{PI}$  control strategy in terms of a) total power penalized and the corresponding b) peak power demand charges per month taking time-of-use periods into account.



**Figure 8.** Yearly evaluation of the simulated control strategies: a) TN effluent concentrations and total energy consumed, and b) Energy cost model versus average energy price.



1

2 **Figure 9.** Impact of the power contracted on the total power term for the different  
 3 strategies evaluated. No bar in Fig 8b means 0 €·year<sup>-1</sup>. Stacked bars in Fig 8c  
 4 correspond to the average of the monthly absolute differences, and the error bars  
 5 correspond to the standard deviation for the 12 months evaluated.

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